

Seismic Behaviour of low-rise Precast Concrete Wall to foundation Connection

Presented by Vinu Sivakumar

Supervisor: Dr. Lucas Hogan

Co-Supervisor: Dr. Rick Henry

1. Slender Precast walls

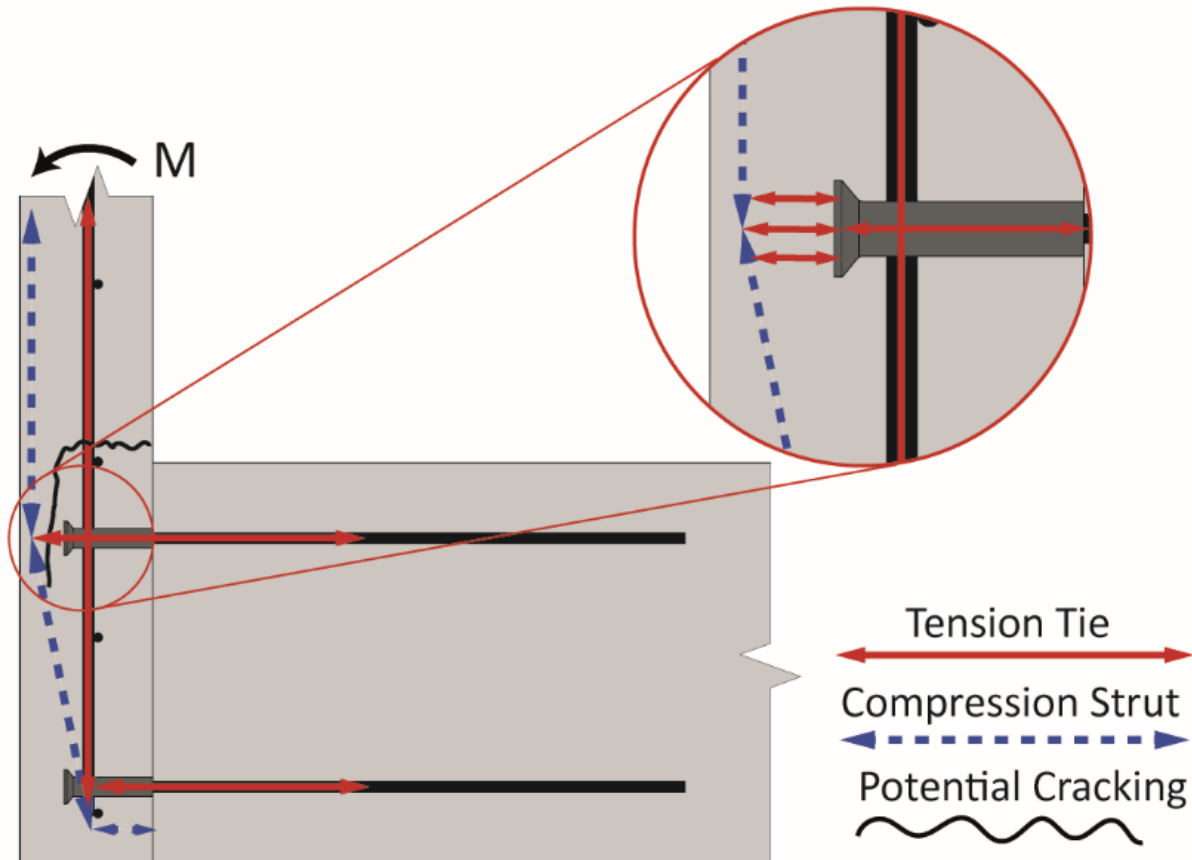
- Extensively used in NZ.
- Commonly used in the low rise structure.
- Essentially act as cladding bracing the building.
- These panels are connected to the foundation by dowel type starter bar-threaded insert connections.



2. SESOC Interim Guidance (2013)

Concrete in tension as part of main load path

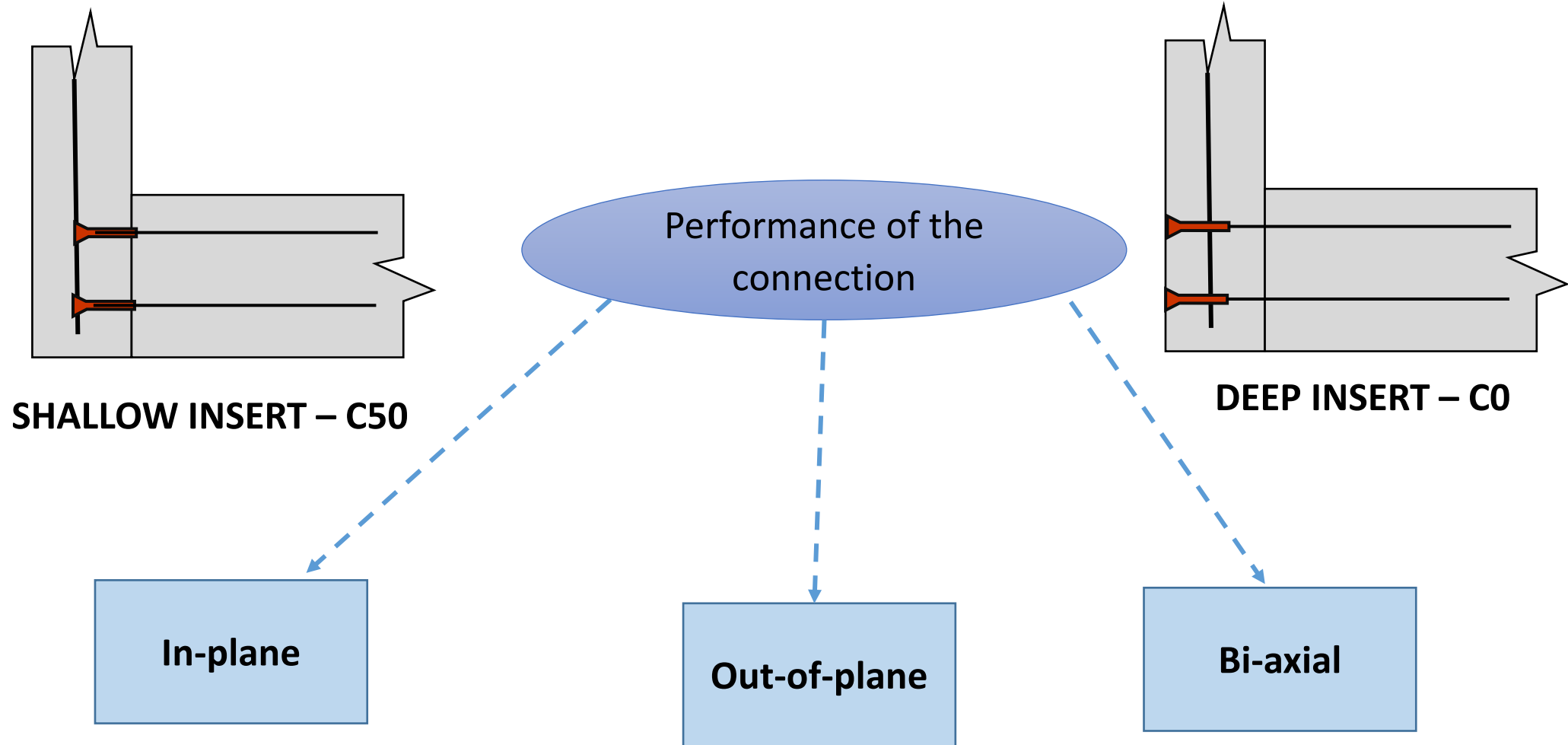
Flexural crack behind the insert and vulnerable under out-of-plane loading



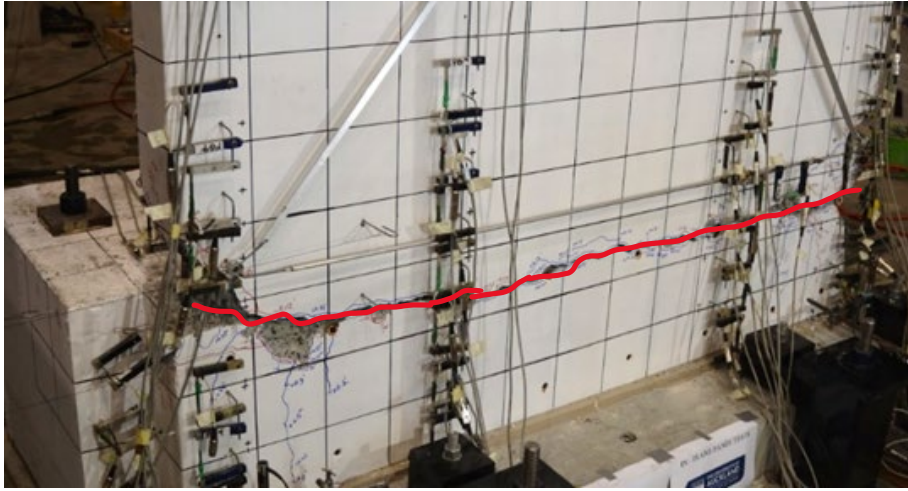
OOP failure



3. Capacity of the connections are they okay?



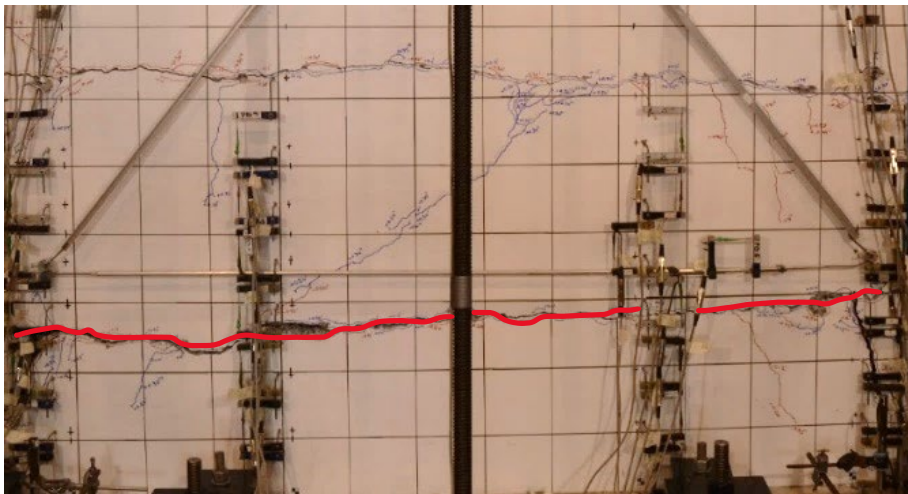
Damage Progression



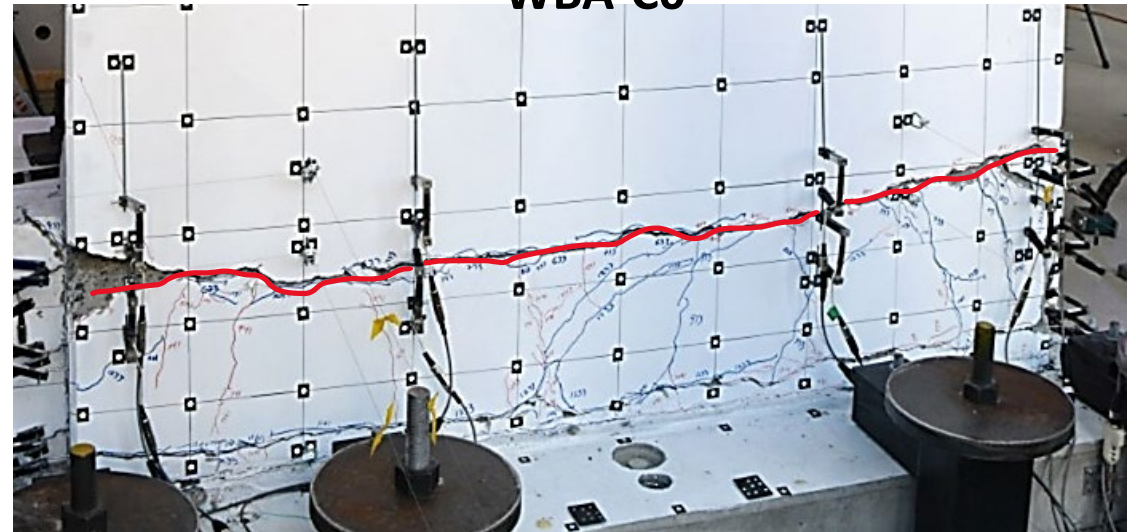
WIN-C0



WBA-C0

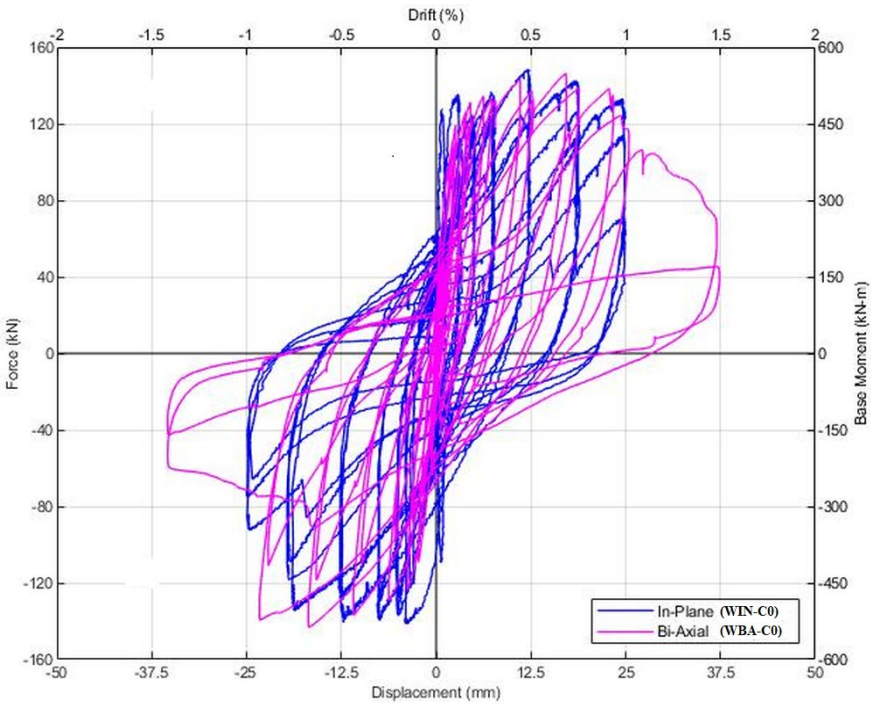


WIN-C50

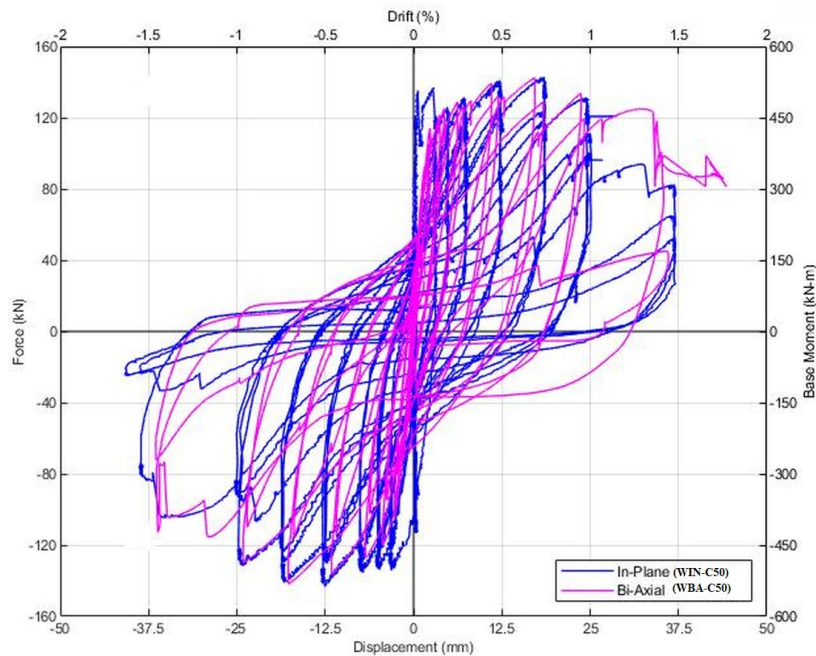


WBA-C50

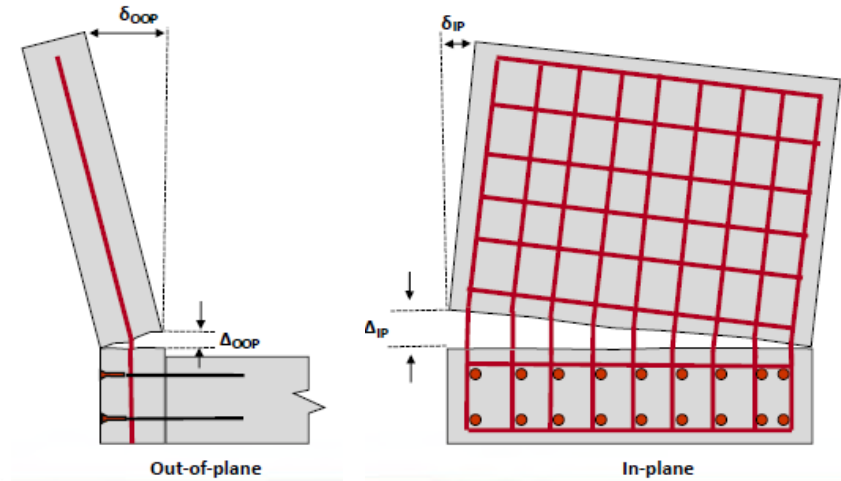
Hysteresis of the panels



Deep inserts



Shallow inserts

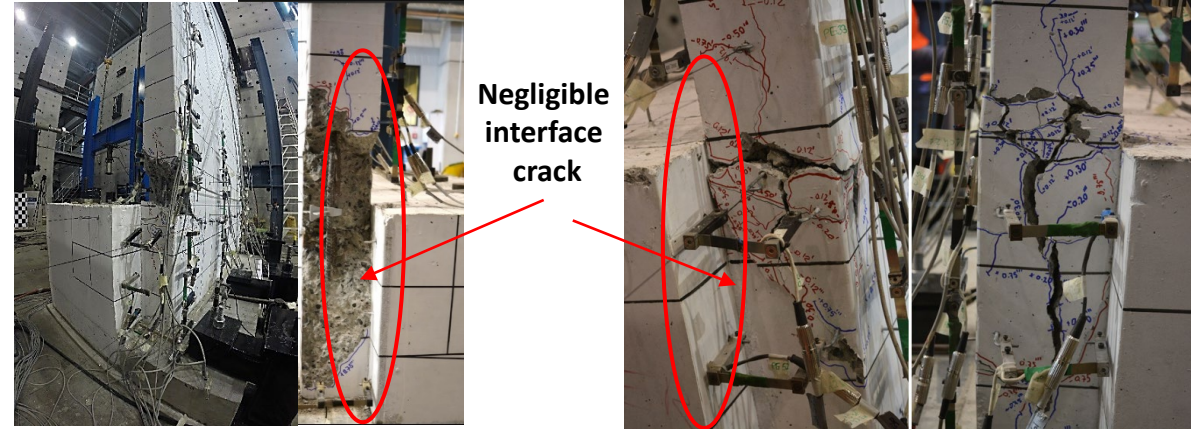
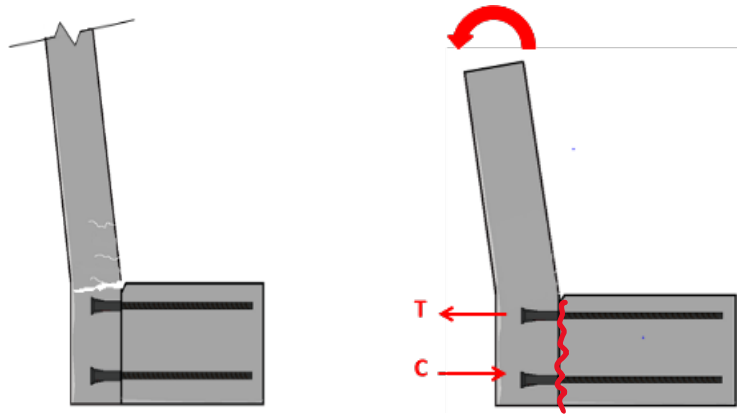


$$\delta_{OOP} > \delta_{IP}$$

$$\Delta_{IP} > \Delta_{OOP}$$

Panel can't close the in-plane crack when loaded in the out-of-plane

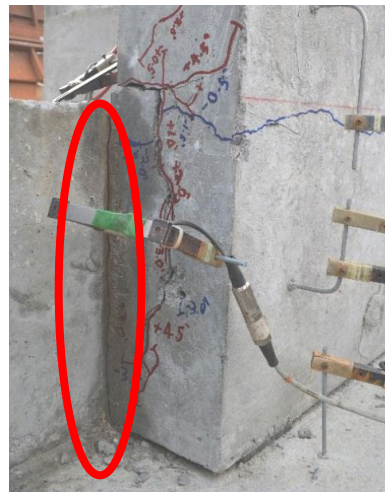
4. Interface crack



WIN-C0

WIN-C50

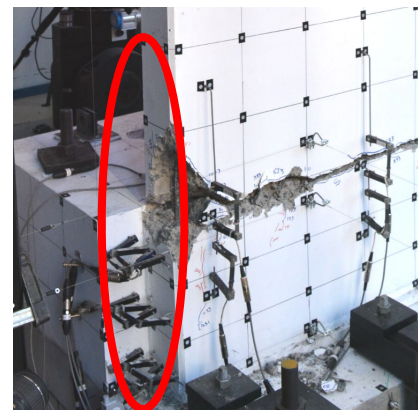
Observed damage by (Gjata et al,2019) – (IN-PLANE)



Panel-TI12-C0

Panel-TI12-C50

Observed damage by (Hogan et al,2018)
(OOP)

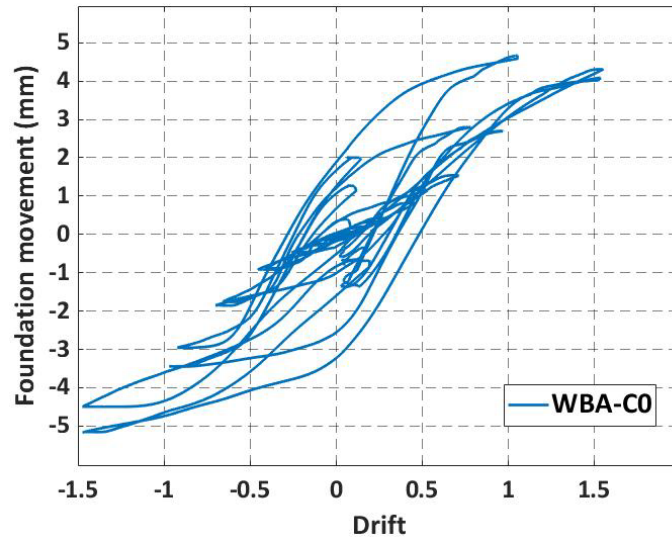
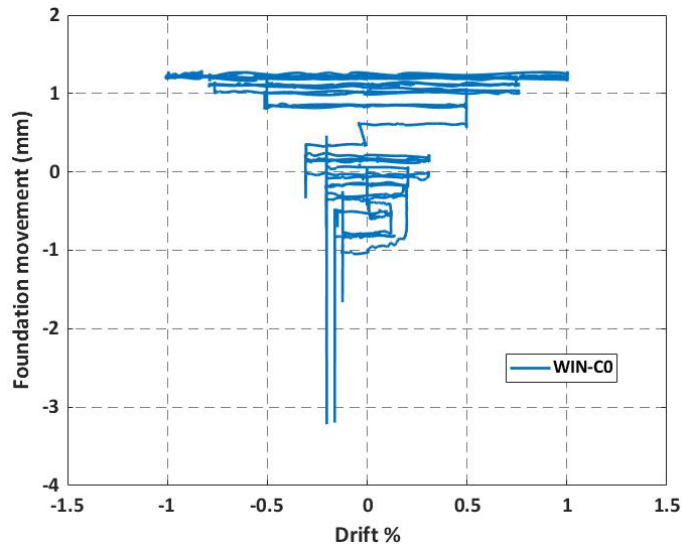
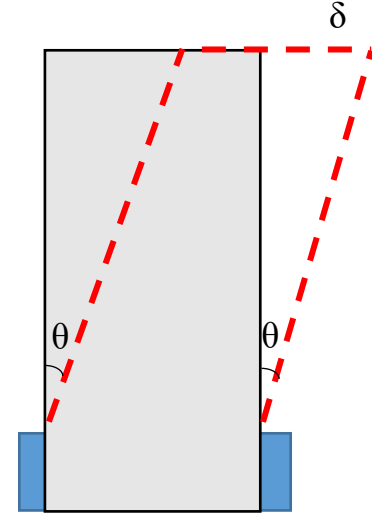
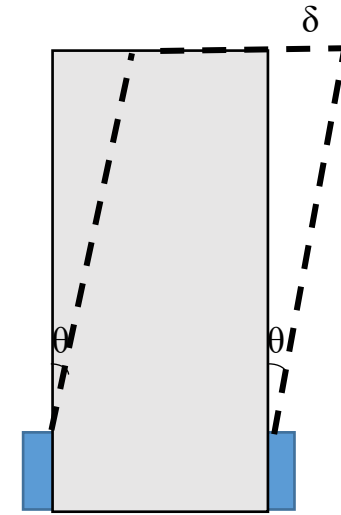
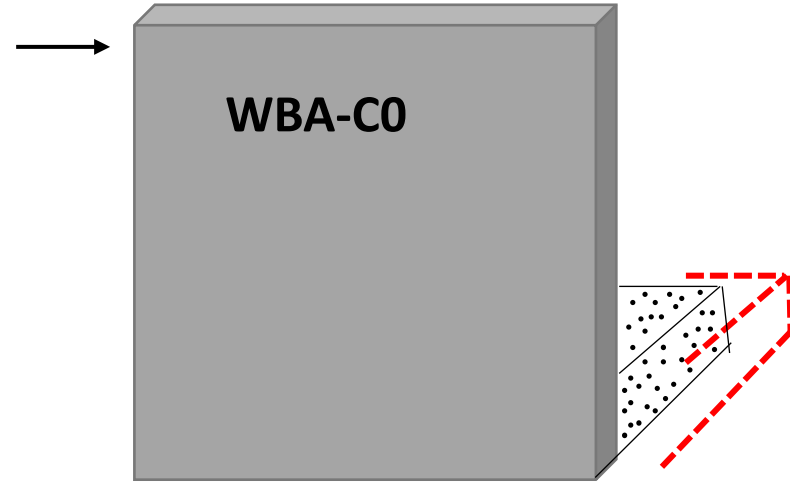
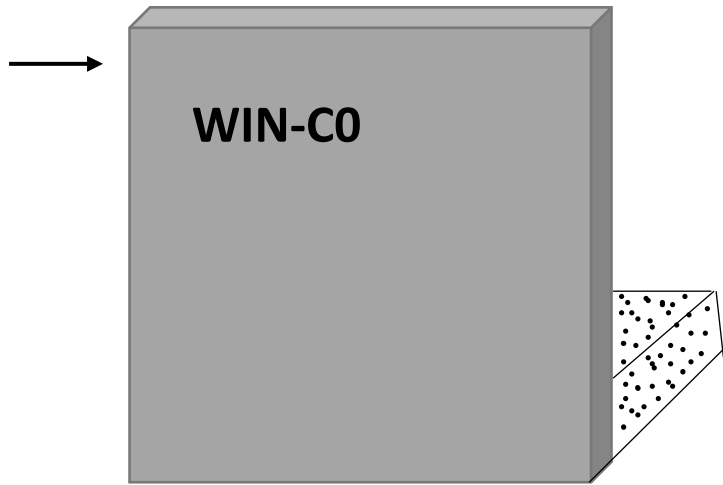


WBA-C0

WBA-C50

Tested by (Hogan et al,2018) – (BI-AXIAL)

Foundation movement



WIN-CO

10 mrad
at 1%

WBA-CO

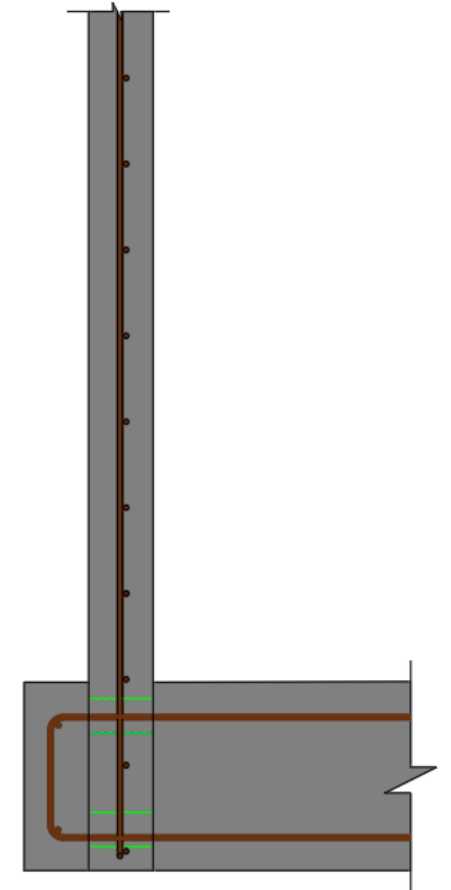
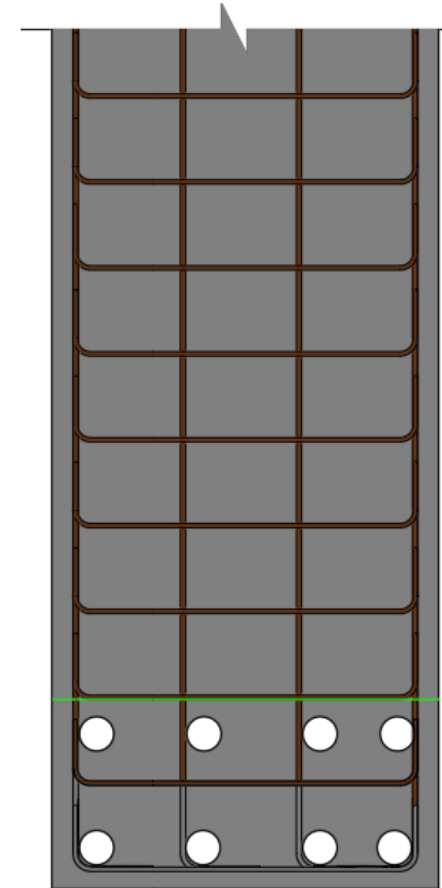
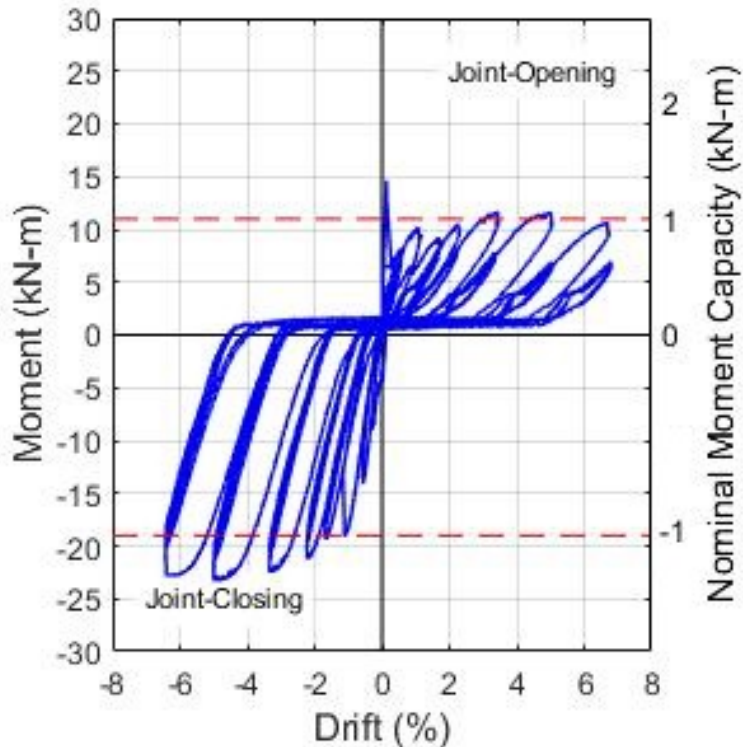
15 mrad
at 1.5%

Is there any alternative connection details?

Proposed Alternative Details

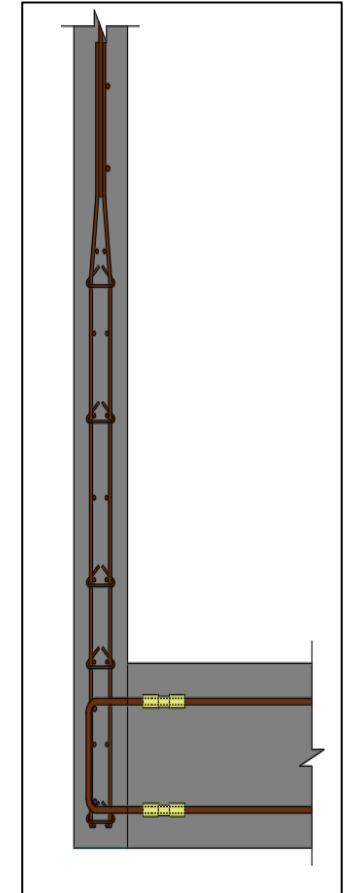
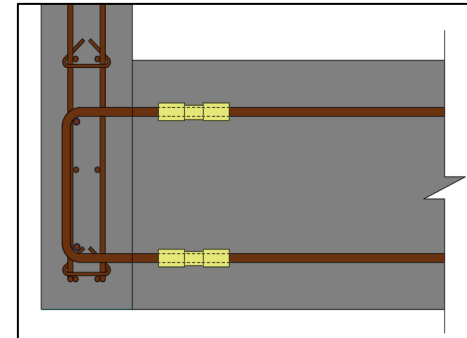
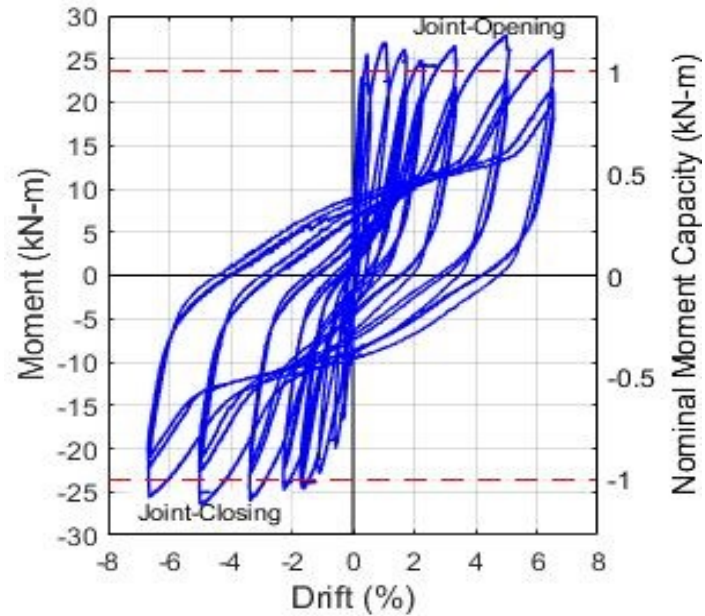
Horizontal Crossbach Detail

It cannot be built if erected on the boundary.

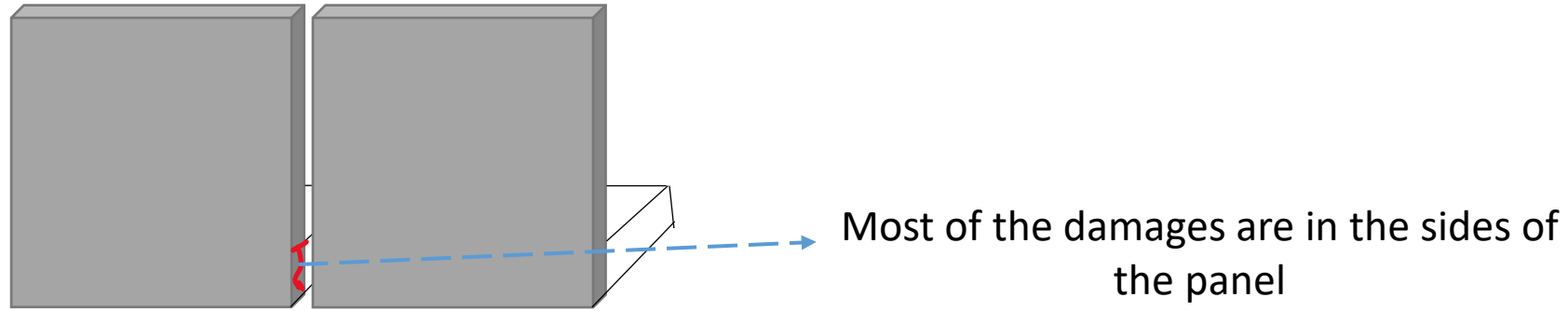


Proposed Alternative Details

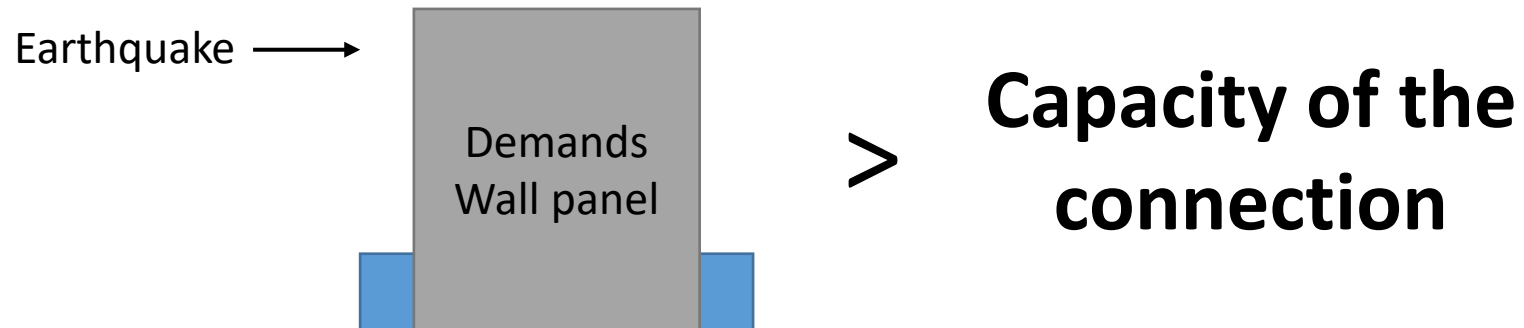
Cranked Bar Detail



(Han et al., 2020)



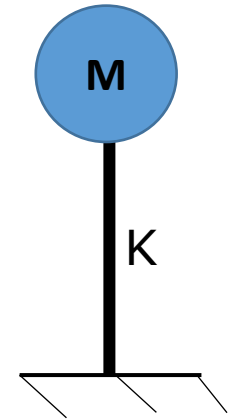
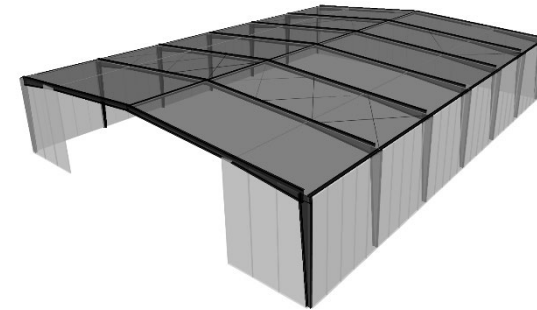
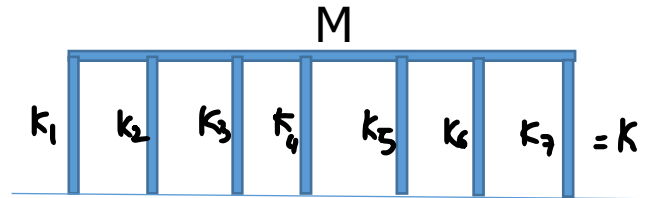
What demands do the buildings are likely to see ?



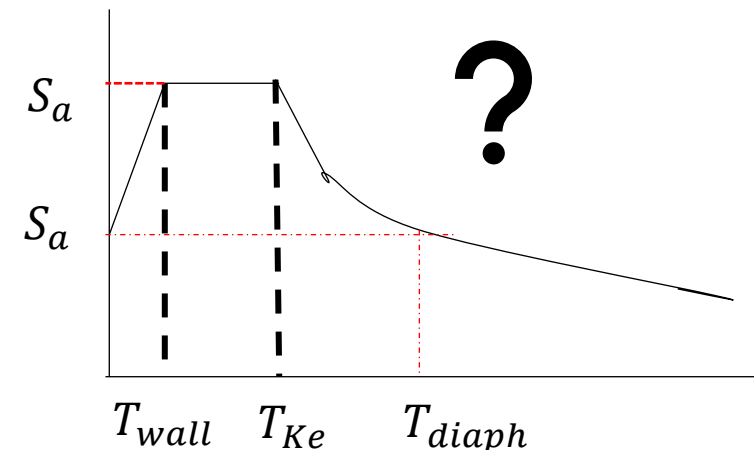
4. Unclear with the response modification coefficient 'R'

- We need to know the stiffness of the wall (k_{wall}) and determine the period T_{wall} of the wall and determine T_{diaph} of the roof.

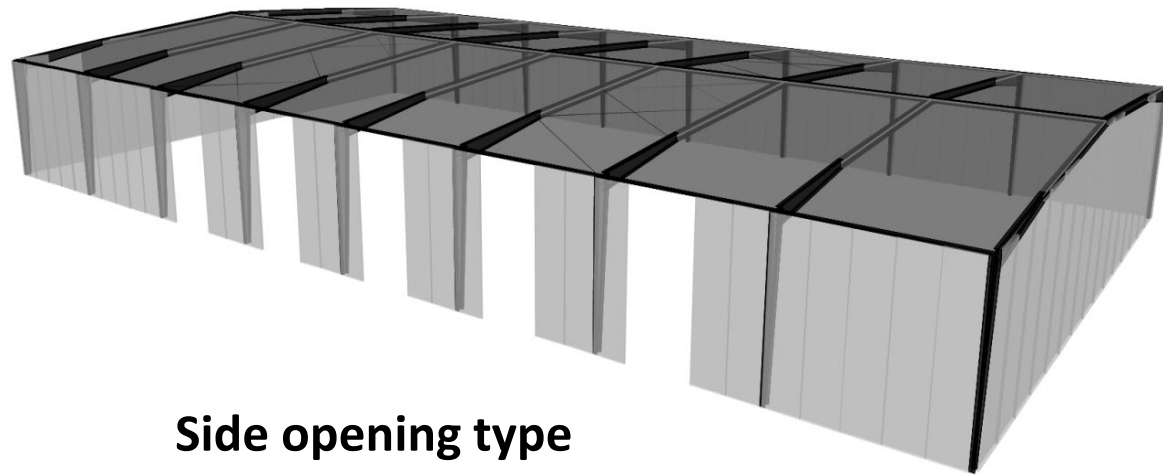
$$\frac{1}{K} = \frac{1}{k_{wall}} + \frac{1}{k_{diaph}}$$



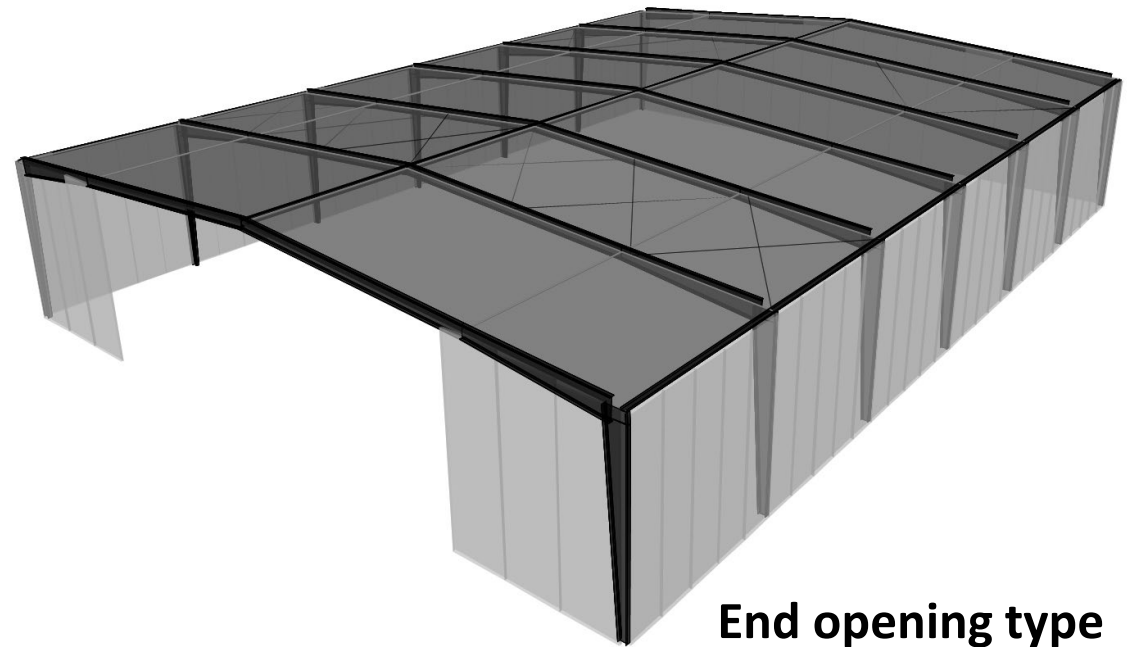
- Additional studies are needed to develop an appropriate response modification coefficient 'R'



3D view of the building typology



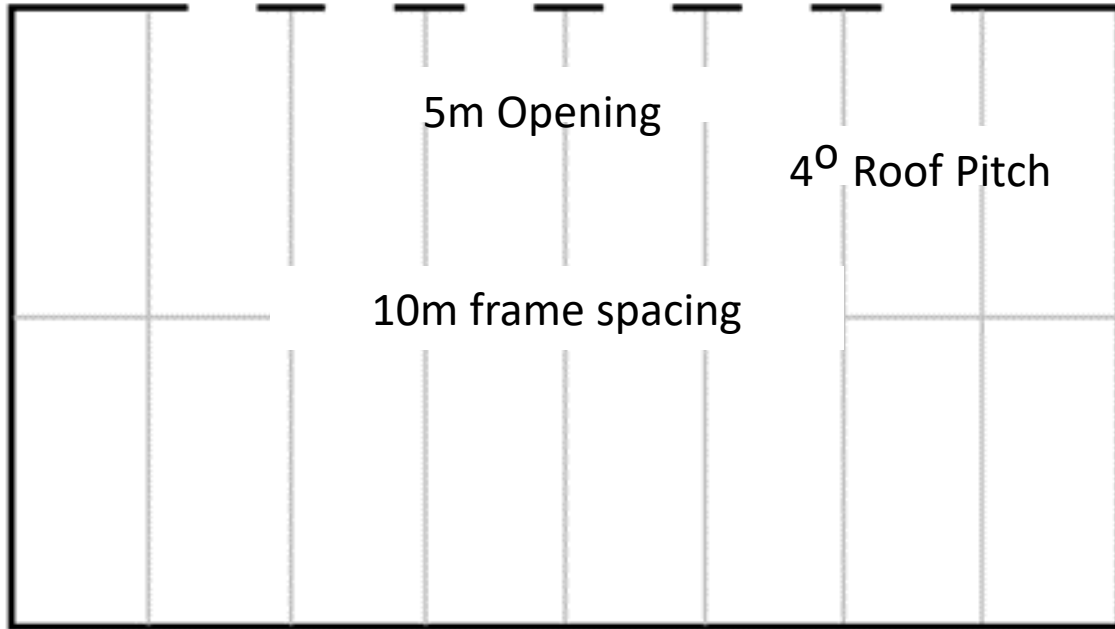
Side opening type



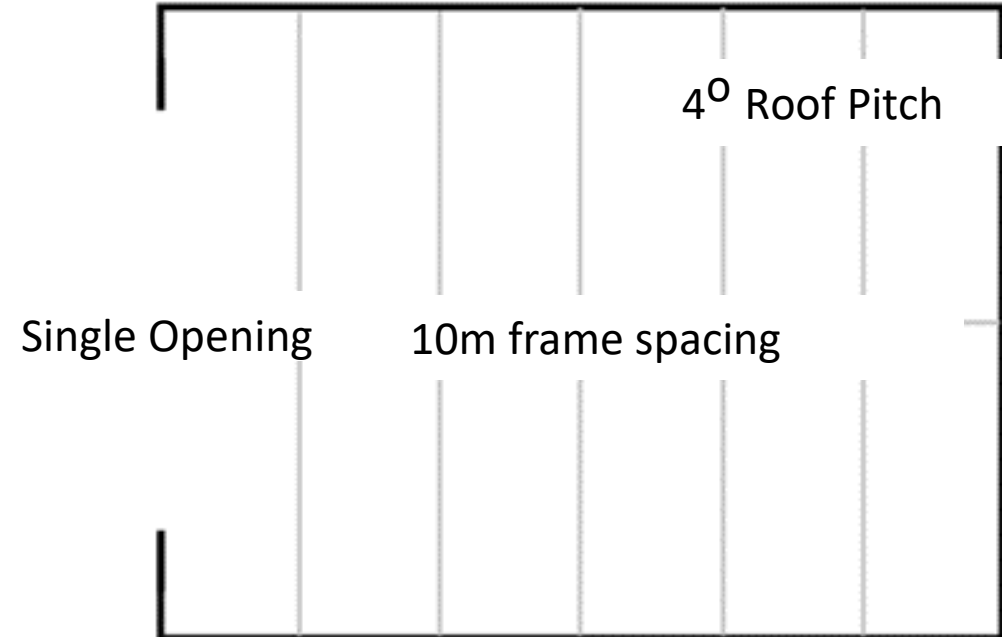
End opening type

Building typology (Hofmann et al., 2016)

Proposed building typology



Side opening type

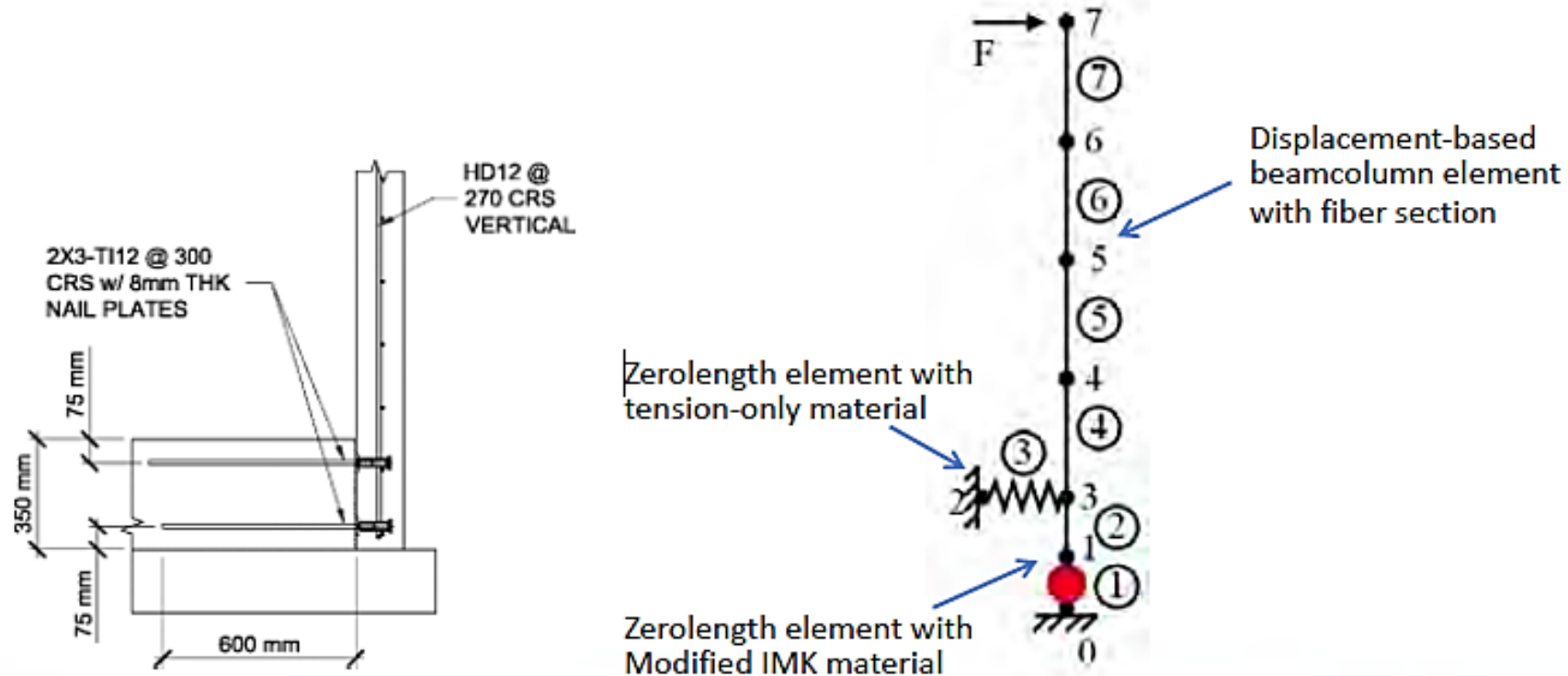


End opening type

	Short span	Mid span	Large span
Side	15m	45m	65m
End	30m	45m	75m

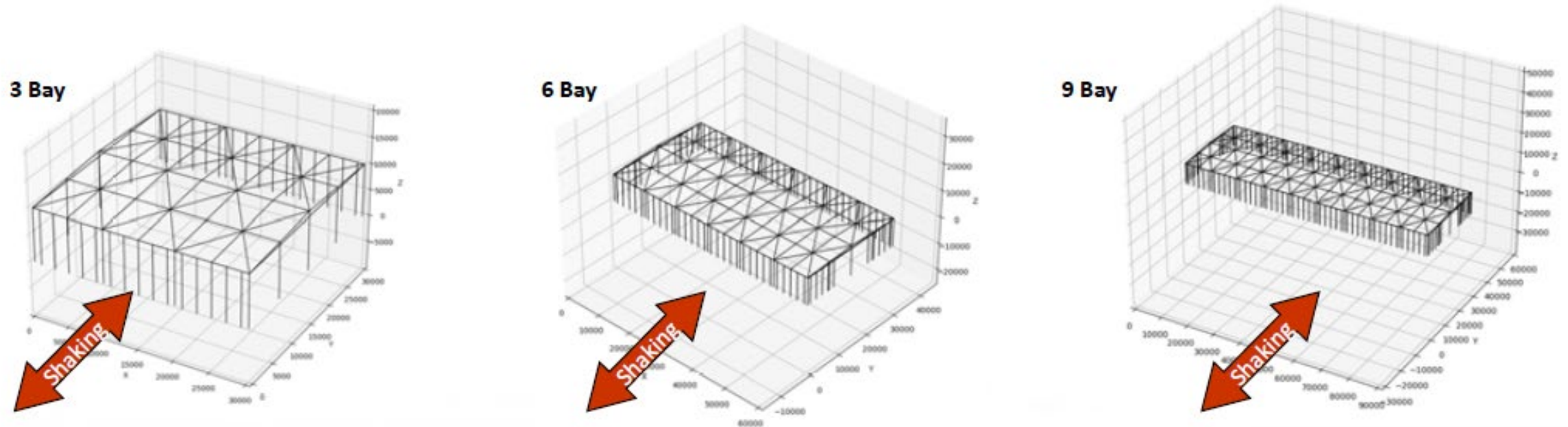
Eave height	Bay spacing	Roof slope	Eave conn
10m	10m	4%	300 PFC

5. System level performance



System level performance by (Liu et al., 2022)

System level performance



- Typical warehouse size 10 m bays, 10m high panels
- Portal frames modeled with lumped hinges
- Flexible diaphragms
- Uniaxial shaking

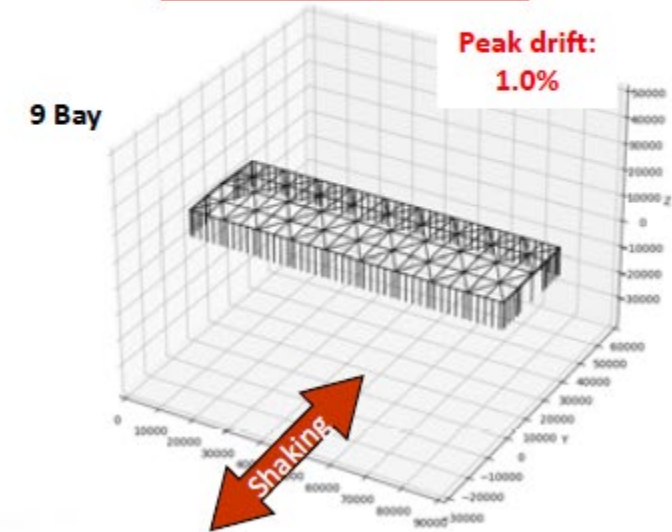
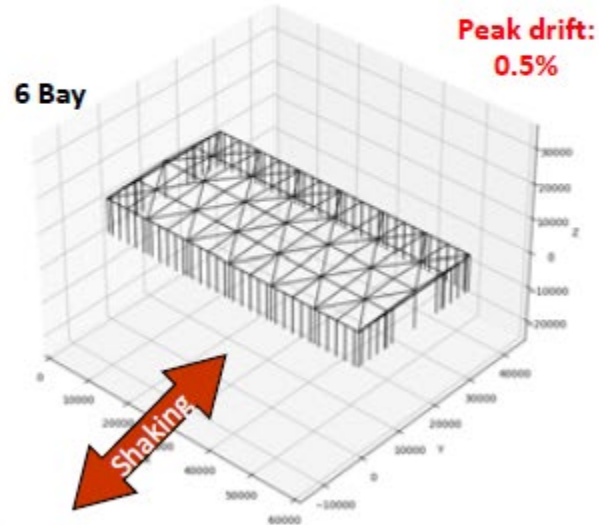
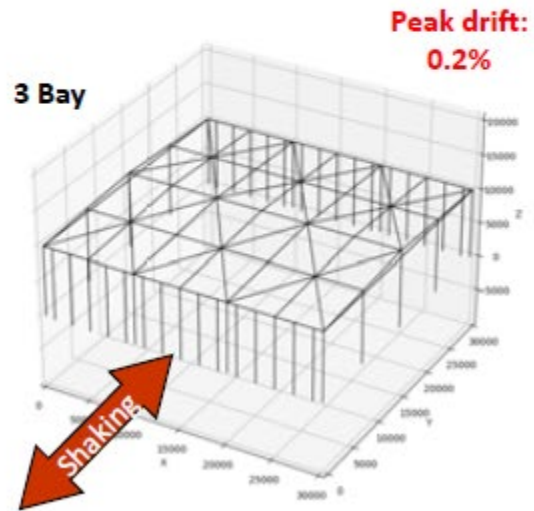
System level performance by (Liu et al., 2022)

System level performance

Joint Rotations < 20 mrad
= no damage

Joint Rotations > 20 mrad
= damage!

Joint Rotations > 20 mrad
= damage!



Joint rotations > Story drift

6. Further investigation

- Alternative connection testing for bi-axial.
- Numerical modelling with the experimental test.
- System level for the different typology of the building model under different loading protocols.



Thank you