

Combining Observed Elastic Basin Amplification Factors with 1D Nonlinear Site Response Analyses

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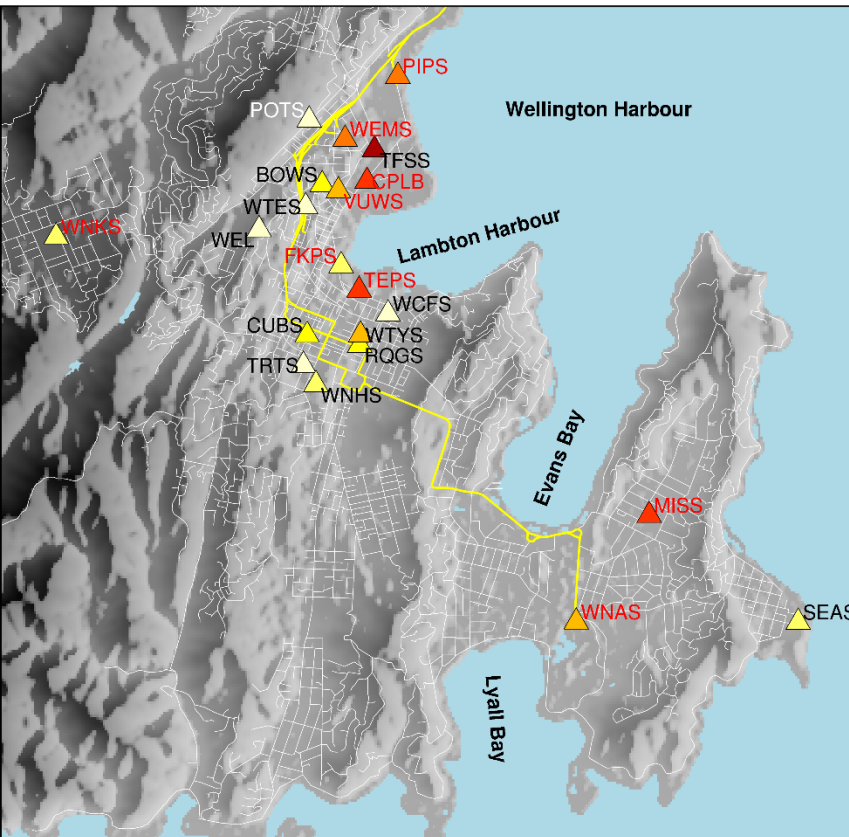


DT1 Meeting
31 March, 2022

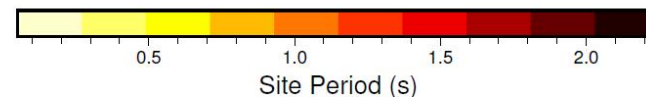
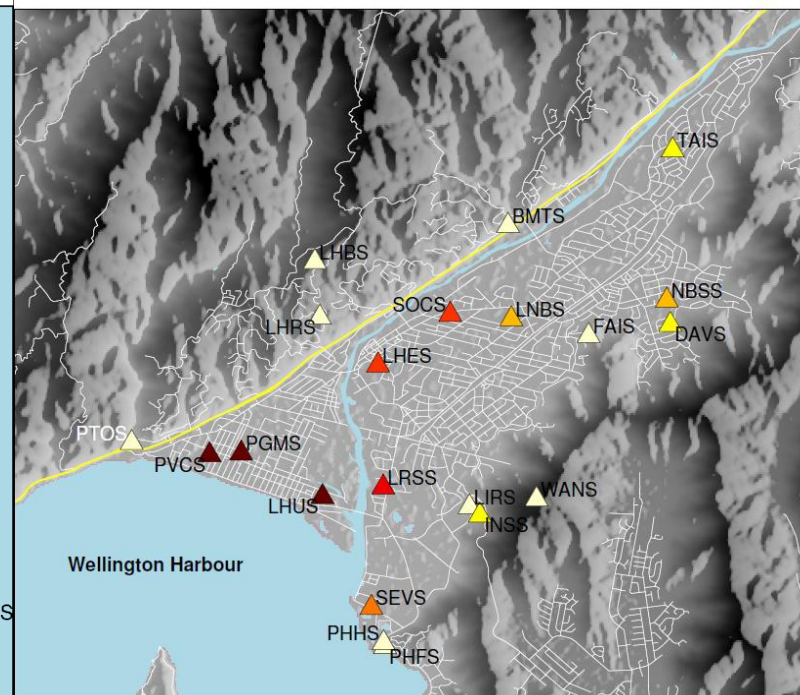


Wellington Basins and Sites Considered

Wellington

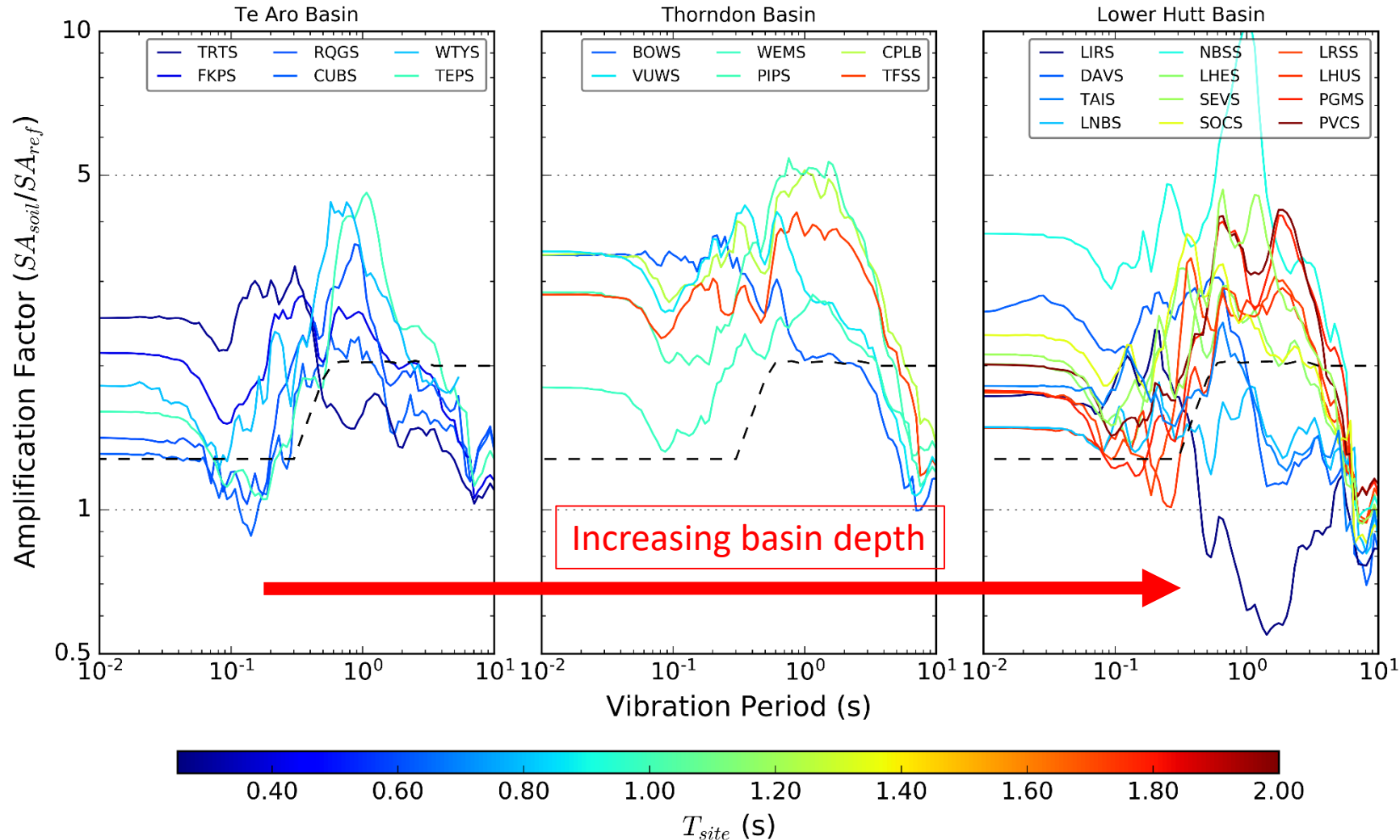


Lower Hutt



- Wellington CBD and Lower Hutt
- 3 basins
- 43 stations
- 9 stations for nonlinear site response

Observed Basin/Site Amplification in Wellington

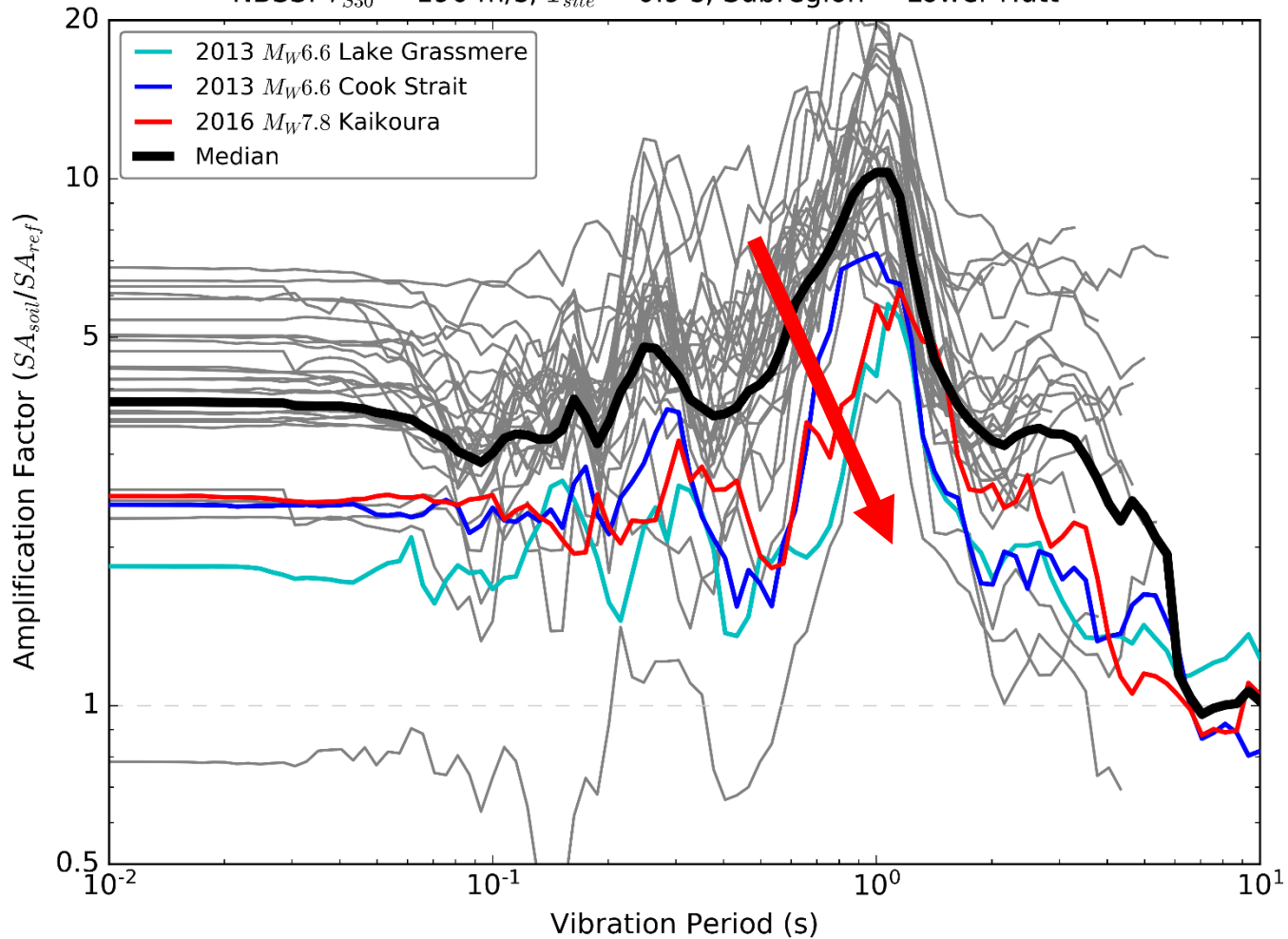


- Average values for each site
- Weak to moderate ground motions
- “Linear” site response

Are these amplification factors reasonable for design-level ground motions?

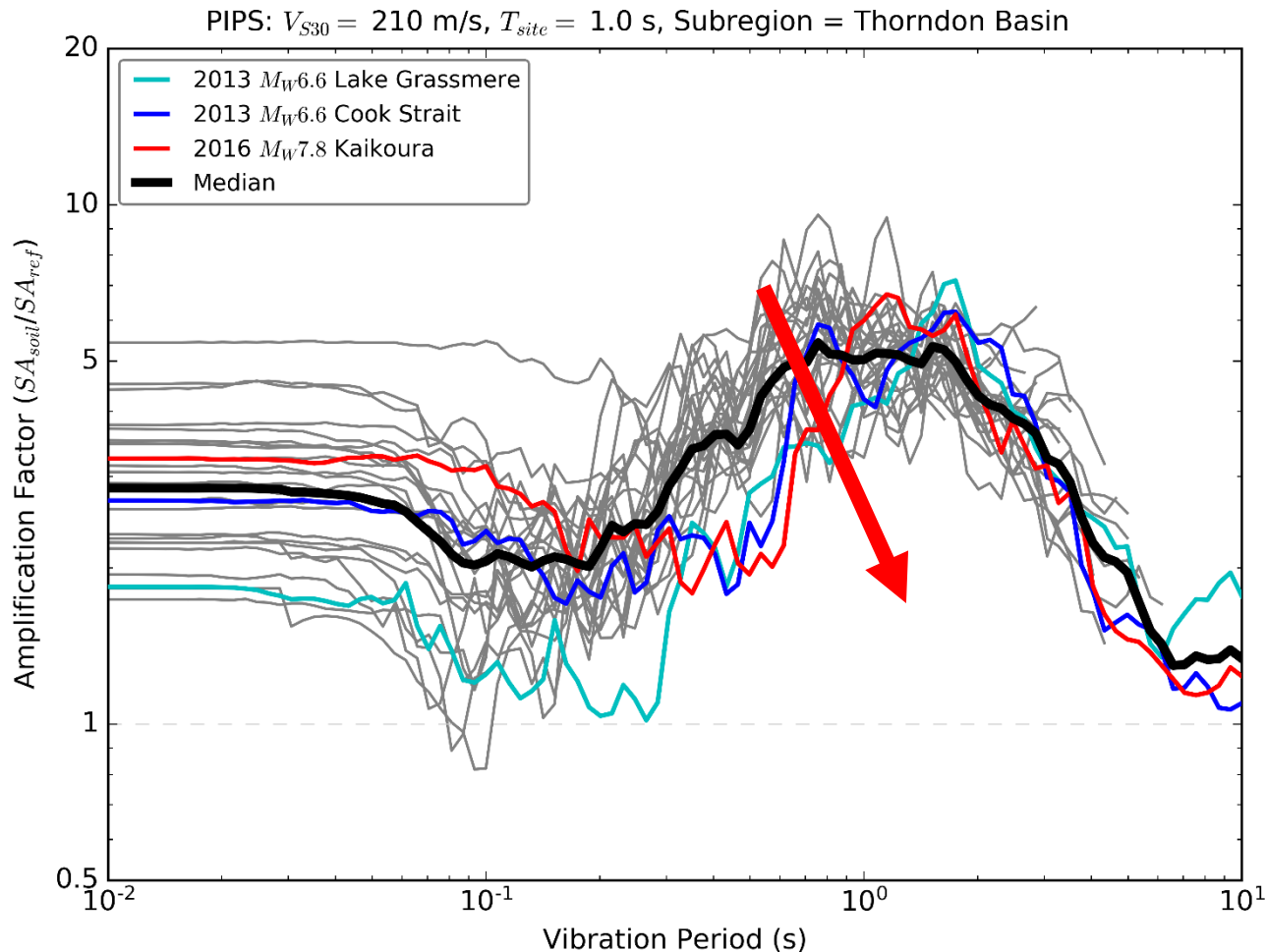
Influence of Nonlinearity on Observations?

NBSS: $V_{S30} = 190$ m/s, $T_{site} = 0.9$ s, Subregion = Lower Hutt



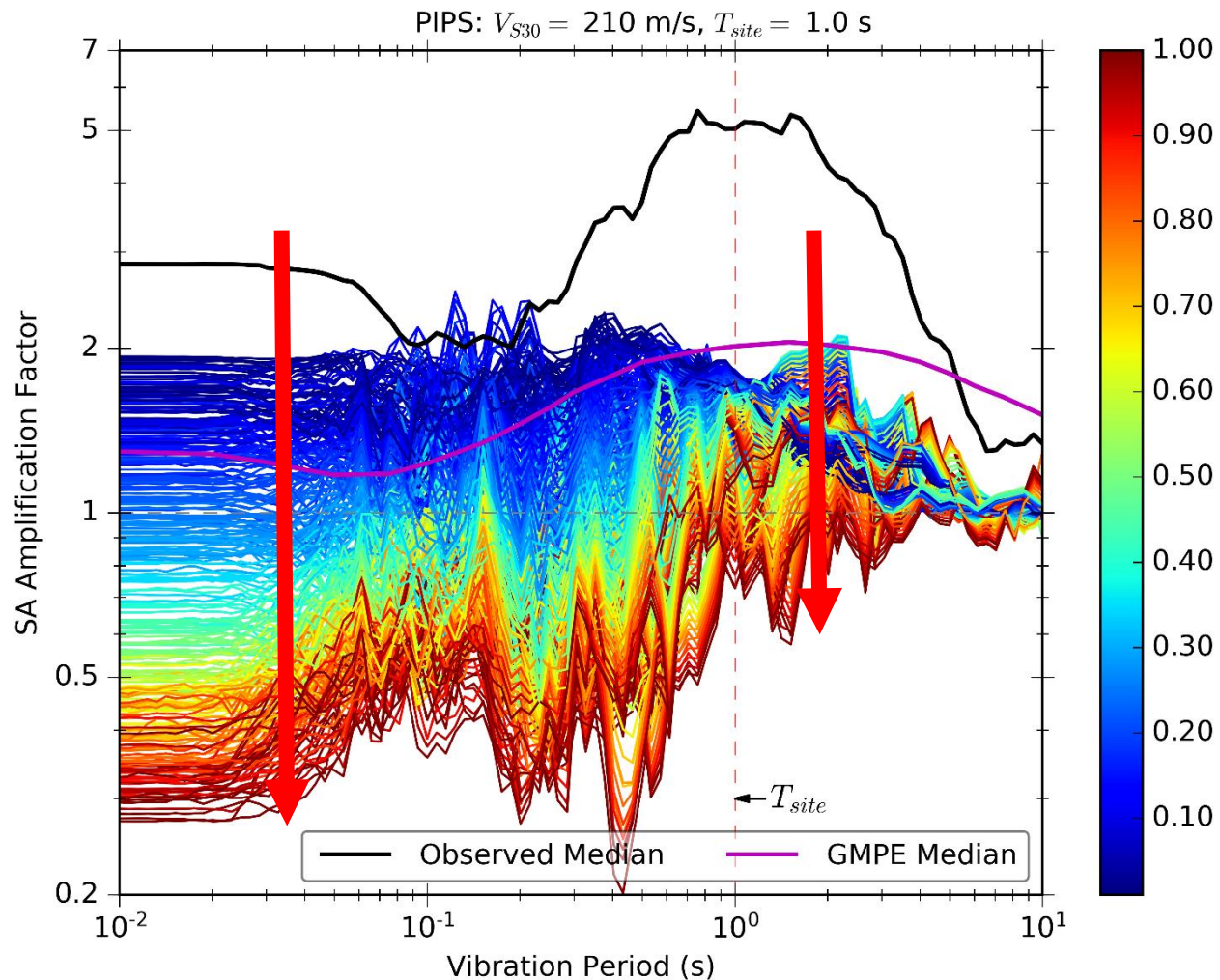
- Observations for all events
- Soft site ($V_{S30} = 190$ m/s)
- Effects of nonlinearity?
- Max $PGA_{soil} \approx 0.2-0.25$ g
- How to validate future events with $PGA > 0.5$ g??
 - Scale 3 large EQs motions up to $PGA^r = 1$ g

Influence of Nonlinearity on Observations?



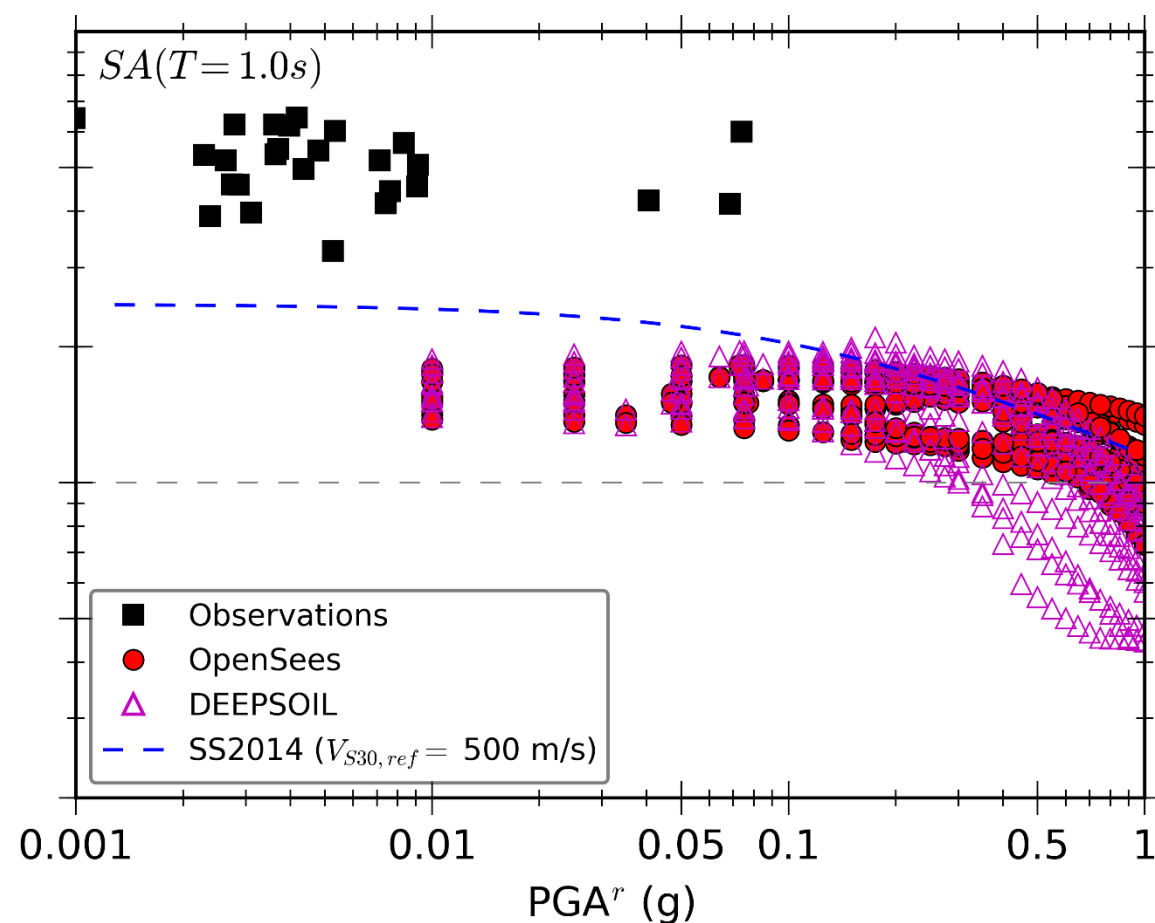
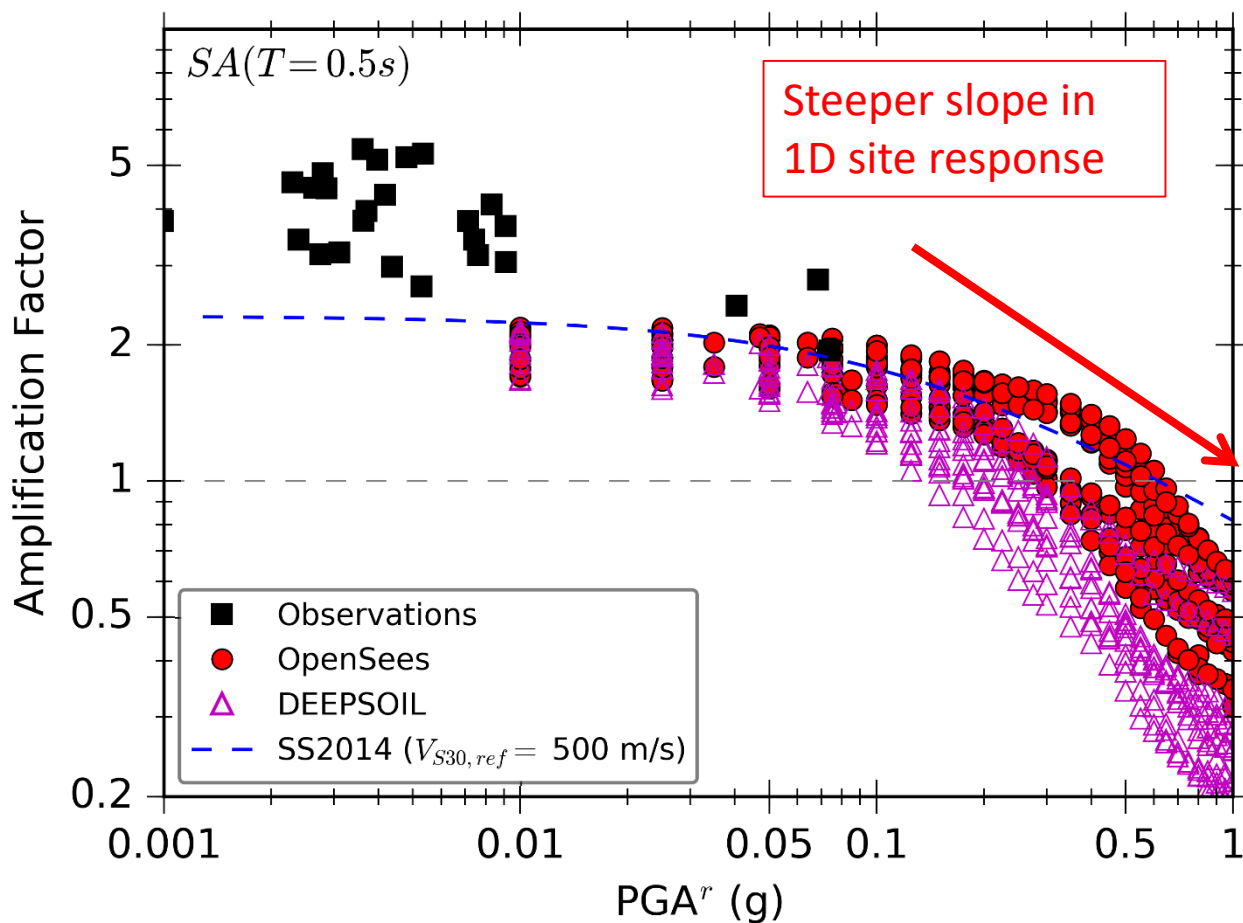
- Observations for all events
- Soft site ($V_{S30} = 210$ m/s)
- Effects of nonlinearity?
- Max $PGA_{soil} \approx 0.2-0.25$ g
- How to validate future events with $PGA > 0.5$ g??
 - Scale 3 large EQs motions up to $PGA^r = 1$ g

Softer Site: PIPS – $V_{S30} = 210$ m/s, $T_{site} = 1.0$ s



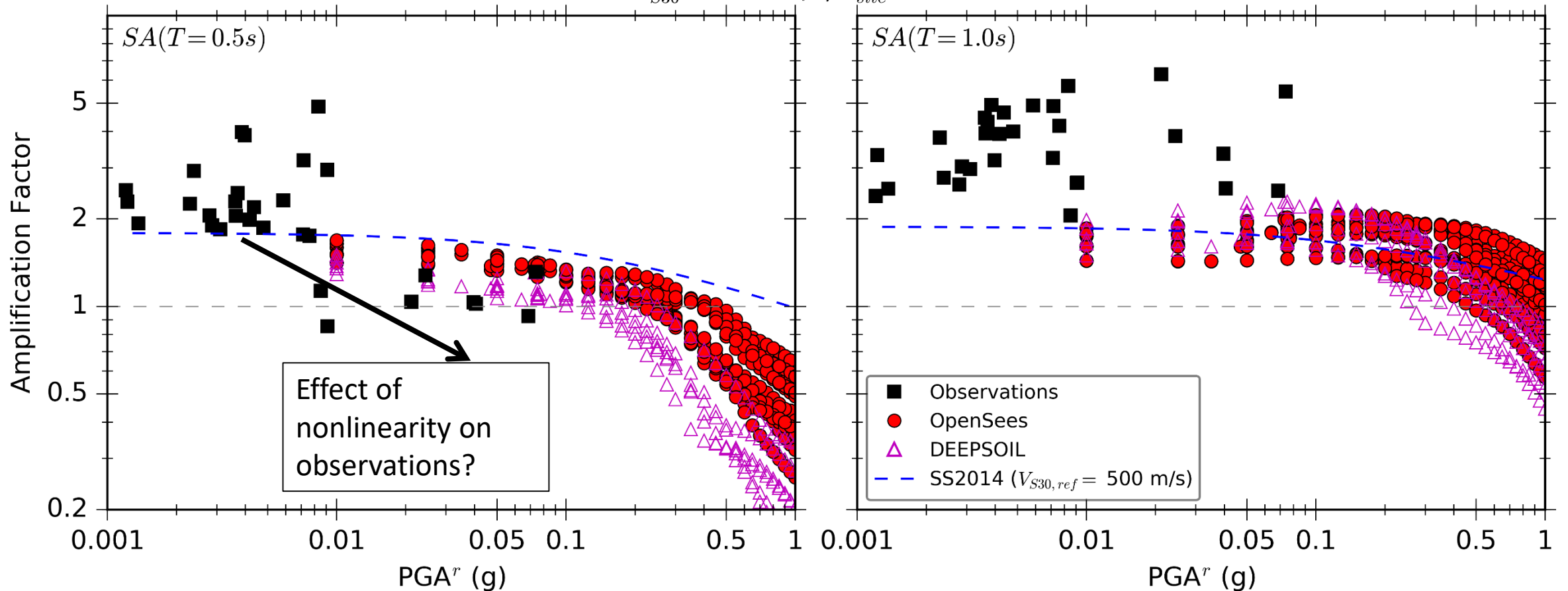
- Scaled input motions
 - PGA^r = 0.01 to 1 g
- 1D analysis doesn't capture basin amplification
- GMPEs don't capture basin amplification
- Significant deamplification at short periods
- Reduction in amplification at long periods.

Softer Site: PIPS – $V_{S30} = 210$ m/s, $T_{\text{site}} = 1.0$ s

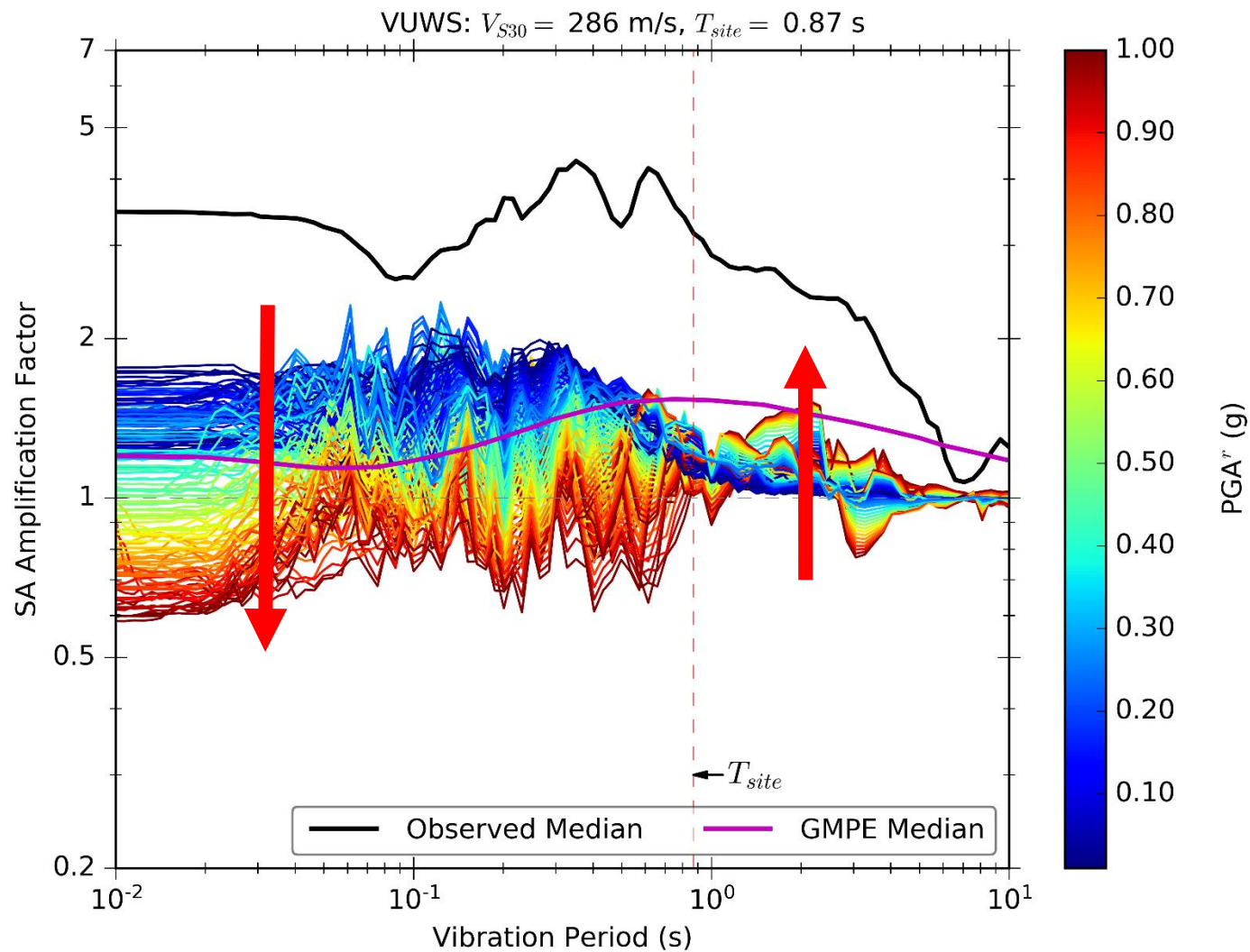


Another Soft Site: Nonlinearity in Observations?

MISS: $V_{S30} = 274$ m/s, $T_{site} = 1.15$ s

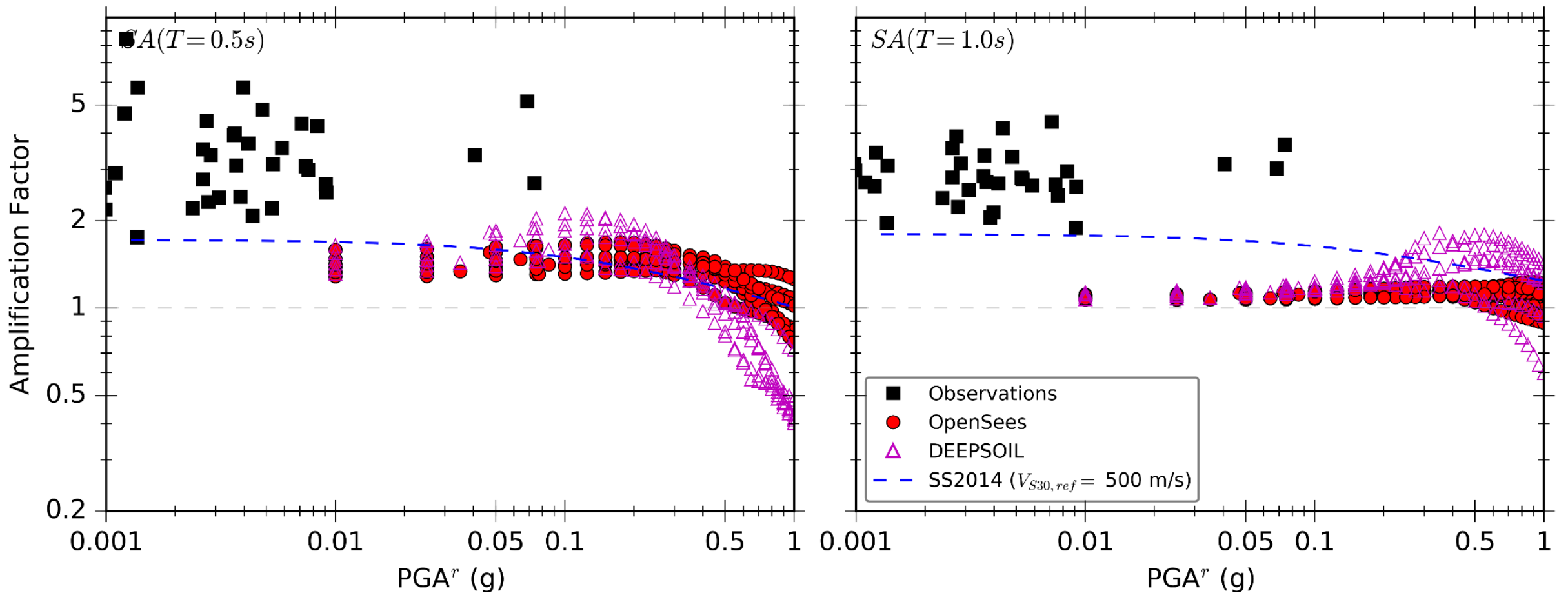


Stiffer Site: $V_{S30} - V_{S30} = 286 \text{ m/s}$, $T_{site} = 0.87 \text{ s}$



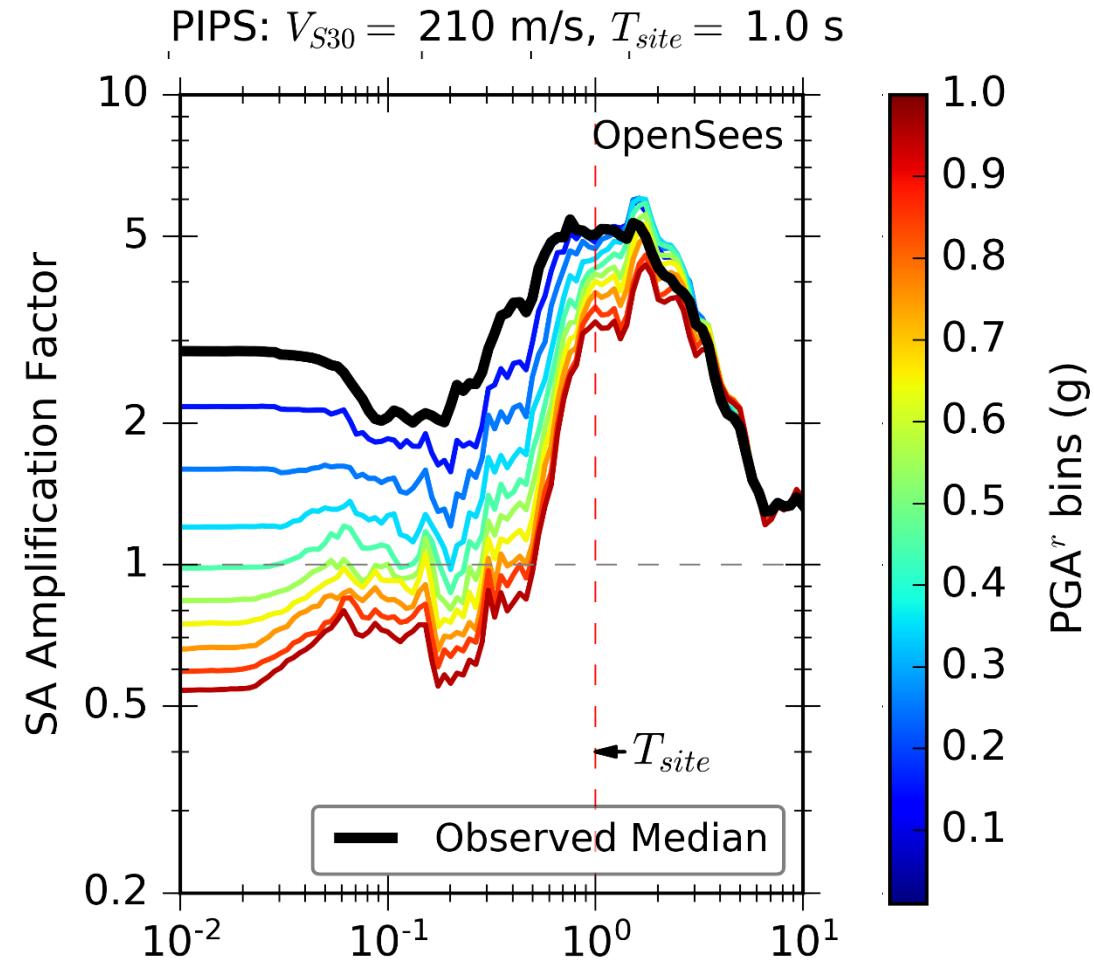
- Less deamplification at short periods
- Increase in amplification at long periods.
- Period elongation from moderate nonlinearity?

Stiffer Site: $V_{UWS} - V_{S30} = 286 \text{ m/s}$, $T_{\text{site}} = 0.87\text{s}$

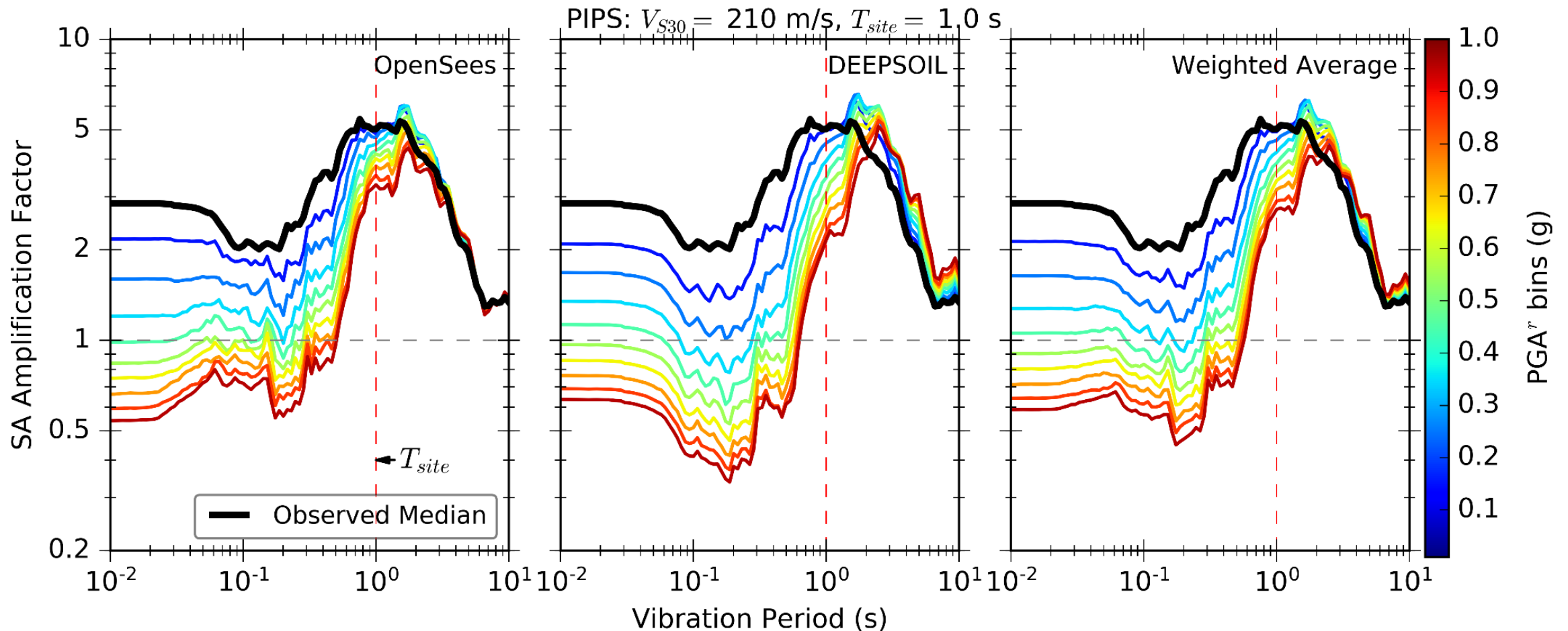


Combining Observations and Analyses

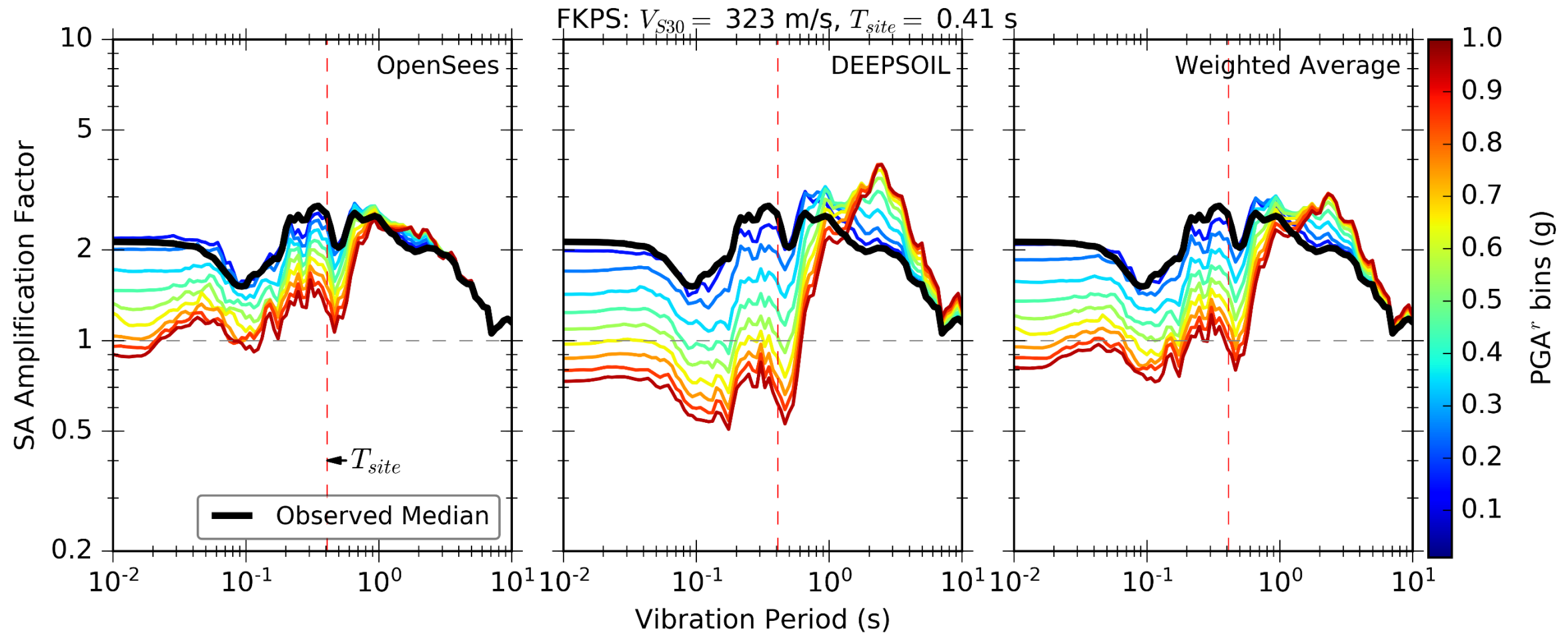
- 1D amplification factors (AF) for $\text{PGA}^r < 0.05 \text{ g}$ \rightarrow “elastic” reference.
- Bin PGA^r into 0.1 g bins.
- Calculate average AF for each bin.
- Nonlinear modifier = $\text{AF}_{\text{elastic}} / \text{AF}_{\text{bin}}$.
- Apply nonlinear modifier to observed median “elastic” site terms



Combining Observations and Analyses: Soft Site Example

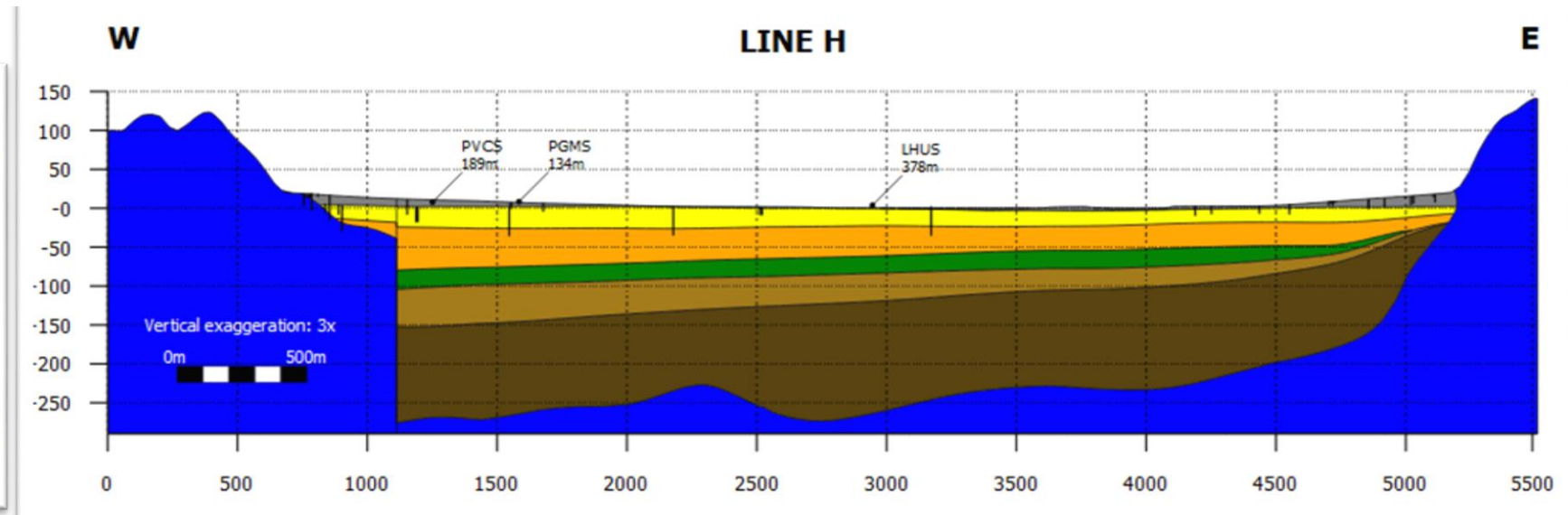
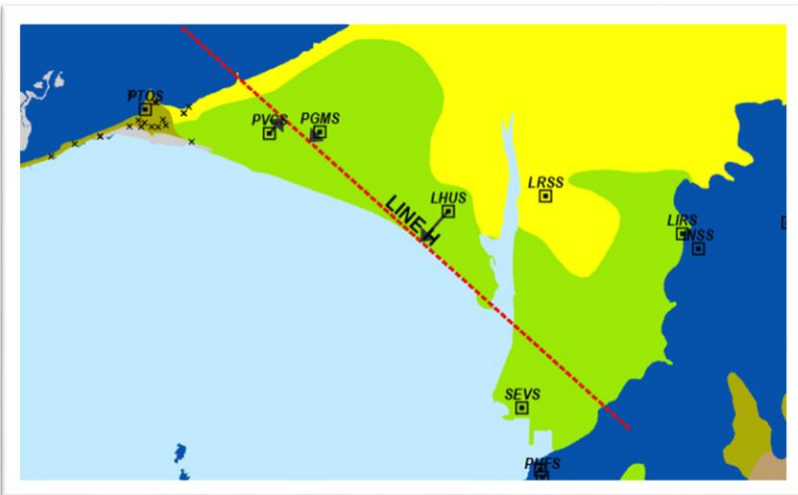


Combining Observations and Analyses: Stiff Site Example



Future Work

- Investigate the coupling between geometric amplification (i.e., basin effects) and impedance amplification/surface nonlinearity.
 - Using 2D nonlinear models
- Assess corrected HVSR as predictor of total site response in Wellington.
 - Basin + Site effects (elastic)
 - Large HVSR database in Wellington



Thank You

Questions?