Developing site-specific high-frequency simulation componentary

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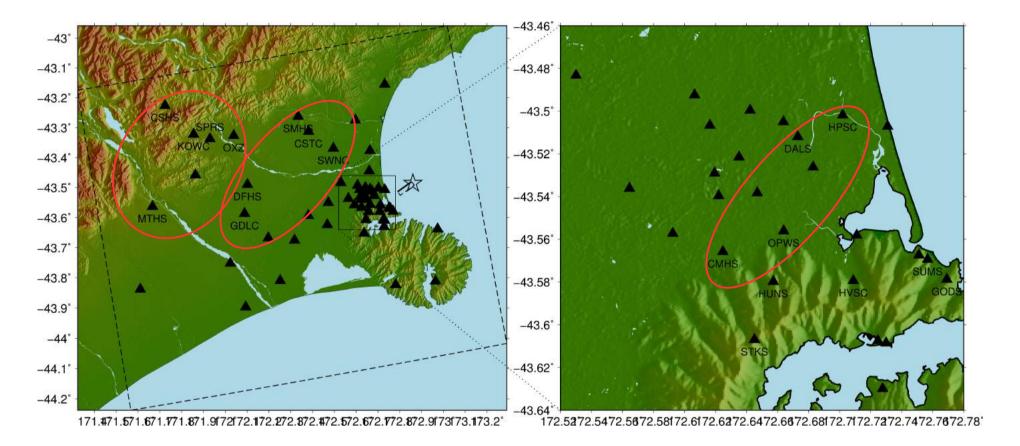
Introduction

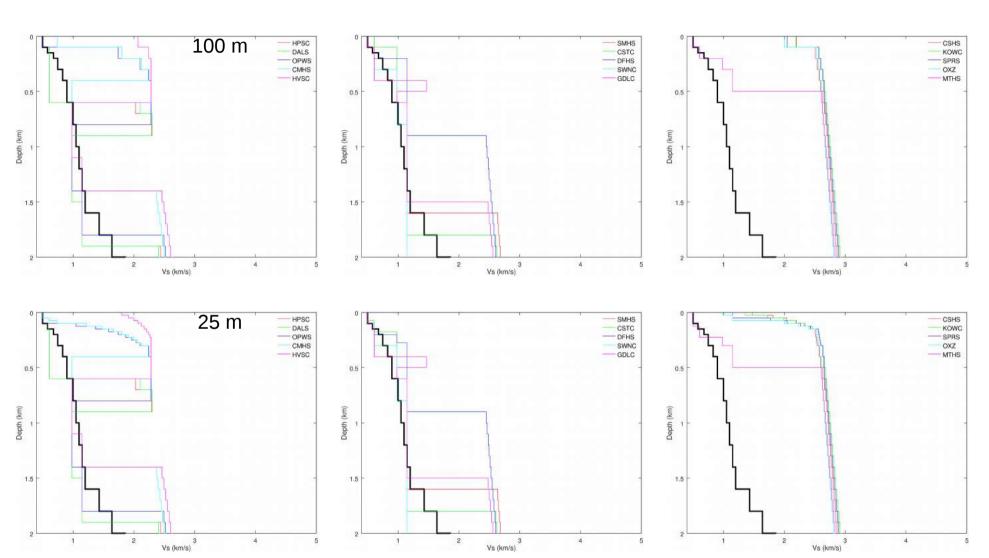
>
$$A(M_0, R, f) = S(M_0, f) * P(R, f) * G(f)$$

[Boore, 2003; Graves and Pitarka, (2010, 2016)]

Use site-specific profiles instead of generic profile.

- \geq Using different profiles affect path and site terms.
- First objective: How site-specific profiles affect site or path or site+path terms and consequently ground-motions.
- Second objective: Apply site-specific method to different earthquakes e.g. 2016 Valentine EQ, 2011 Christchurch EQ, 2010 Darfield EQ.







Site term

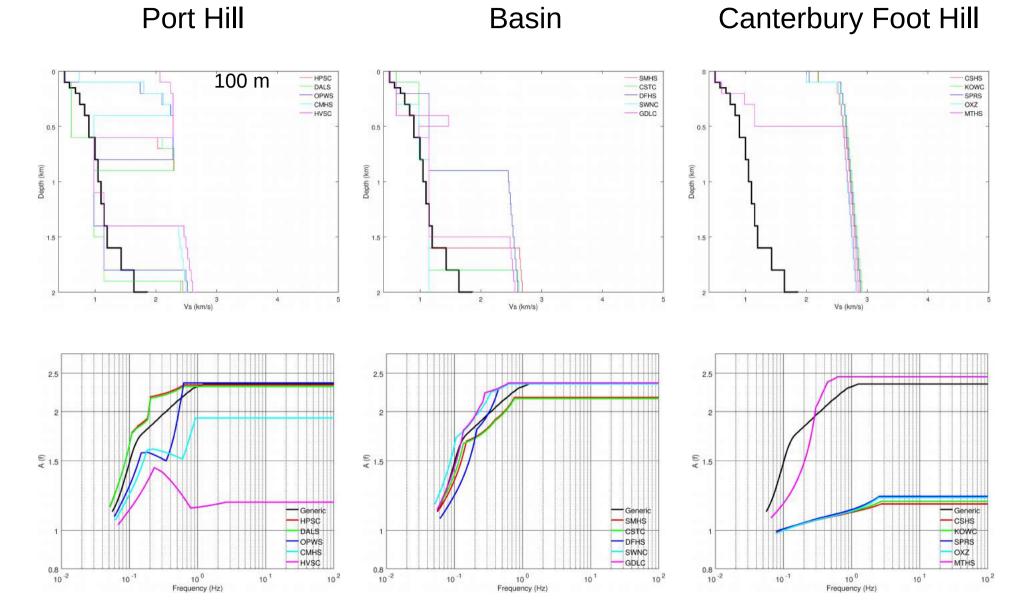
G(f) = A(f) * D(f)

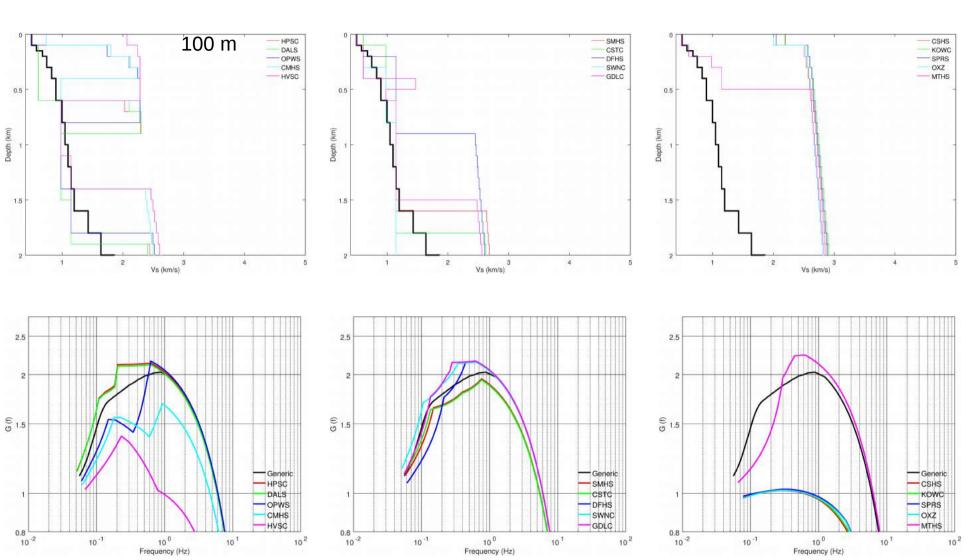
[Boore, 2003]

> A(f) is computed using "quarter wavelength theory".

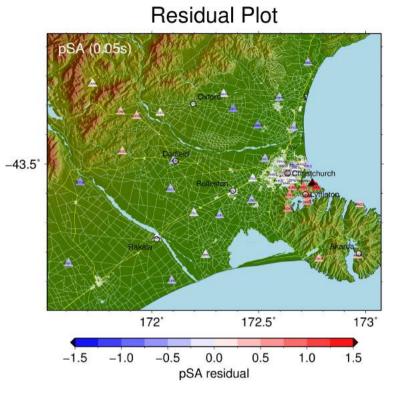
A(f) = Square root of ratio of source to site impedences. [Boore and Joyner, 1997]

D(f) = exp(-pi * k * f)

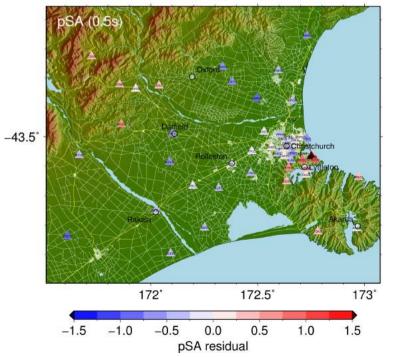




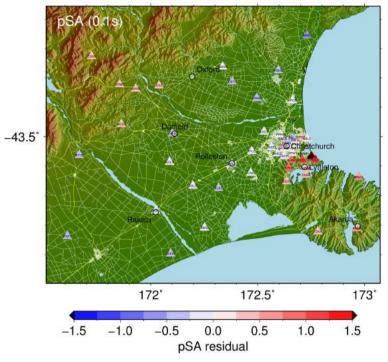




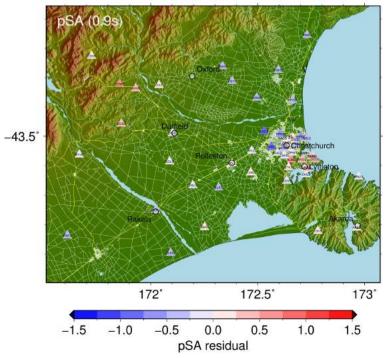
Residual Plot



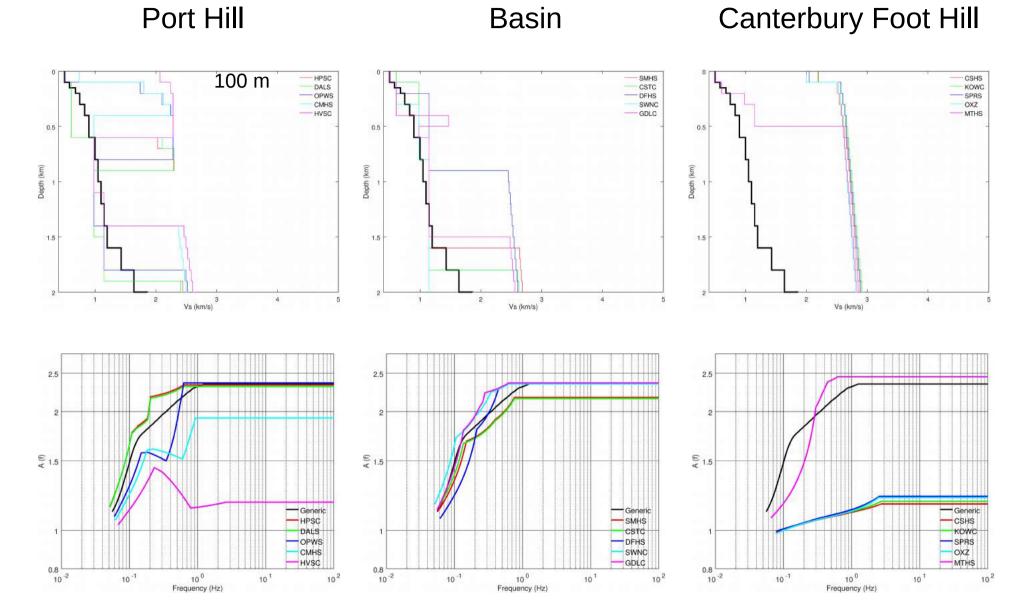
Residual Plot



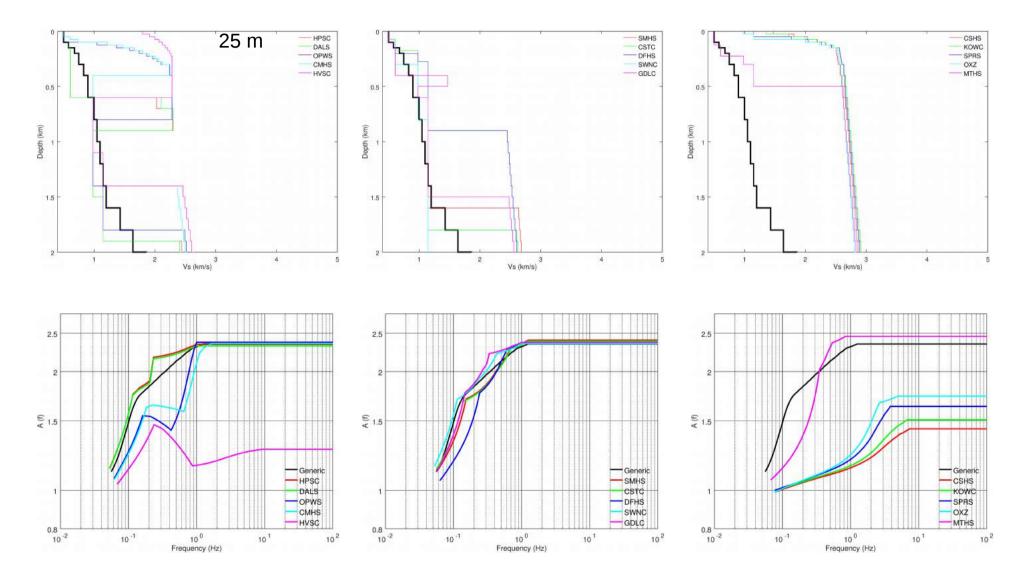
Residual Plot



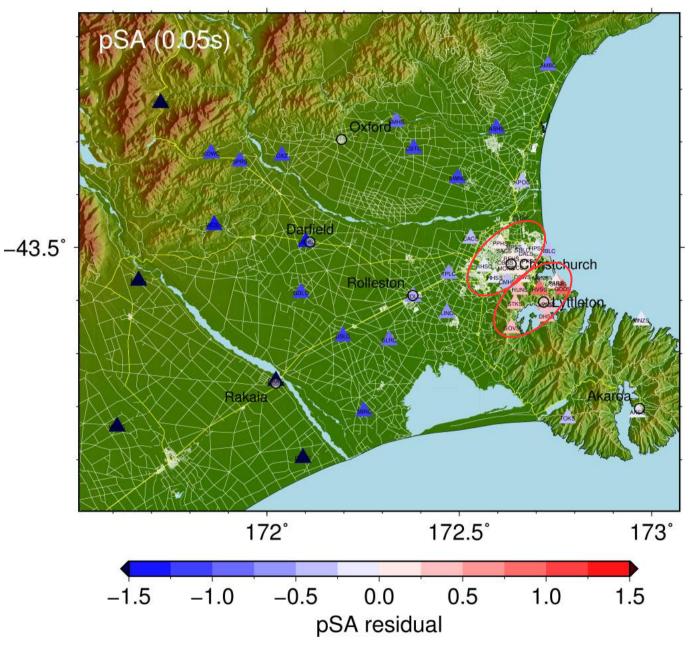
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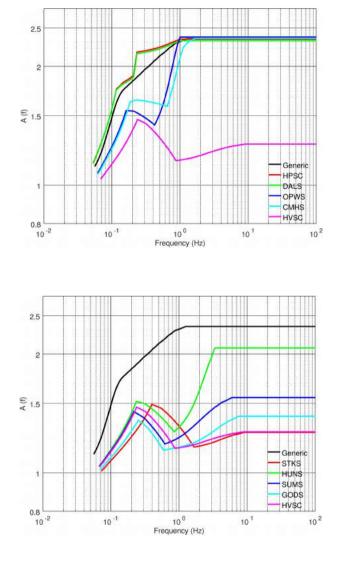






Residual Plot





Summary:

- > We understand/evaluate how the different 1D velocity profiles affect the site term and consequently ground-motions.
- Velocity variations in top 300 to 500 m depth significantly affects the site amplification/term (depicts the importance of weathering function).

Future work:

- \geq Need to better understand combined path and site components.
- Apply to different earthquakes to show/check the improvement in ground-motion estimation.

<u>Thanks</u>

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