National-scale infrastructure network exposure to liquefaction using geospatial models

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ABSTRACT

Liquefaction hazard maps are a useful resource to help estimate the exposure and potential liquefaction-induced damage to the built environment. The most robust approach for the development of these maps is through the use of in-situ investigation data and simplified liquefaction evaluation procedures. When infrastructure networks are the focus of assessment, this method can be expensive and labour-intensive due to the large geospatial extent of these networks and the large number of investigation data required to provide good coverage. In these cases, geospatial methods can be used as an alternative approach. This paper focusses on the assessment of the exposure of New Zealand's transportation (rail, state highways, and bridges) and power transmission networks to liquefaction, using geospatial liquefaction susceptibility methods. This approach has enabled the initial quantification of national exposure across each network for different liquefaction susceptibility categories, demonstrating that transportation systems are situated in areas that are more susceptible to liquefaction compared to power transmission facilities. To identify areas of high risk in terms of liquefaction induced damage, susceptibility needs to be linked with the seismic hazard across the country; this is the focus of the next step of this research. The criticality or significance of infrastructure should also be considered as part of this process to better quantify the impact of damage to the wider economy and society. This includes the modelling of other infrastructure networks, such as local roads, and the analysis of links between networks and areas of interest, such as populated places and sea ports.

Keywords: liquefaction, geospatial methods, infrastructure, New Zealand, exposure assessment

1 INTRODUCTION

Liquefaction during seismic events can lead to significant damage to buildings and infrastructure networks, including differential settlement of buildings, distortion of roads, or breakage of buried infrastructure (Mian et al., 2013). Because of its young coastal sediments and its location along the Pacific Basin Ring of Fire, New Zealand is prone to liquefaction induced damage. During the 2010-2011 earthquakes in Christchurch, liquefaction and lateral spreading led to significant damage to the built environment; it affected around 60 000 residential houses and severely impacted lifelines and infrastructure within the city (Cubrinovski, 2013).

An effective resource to identify areas of risk and to estimate the potential extent of damage to buildings and infrastructure is a liquefaction hazard map. However, the development usually requires extensive investigation to characterise the potential liquefaction-induced damage using simplified liquefaction evaluation procedures. Common in-situ site investigation methods to obtain this information are the Standard Penetration Test (SPT) or Cone Penetration Test (CPT) (Boulanger & Idriss, 2014; Zhu et al., 2017). When assessing distributed infrastructure networks, the number of investigations required can be expensive and labour-intensive, hence they may not be suitable for the overall assessment of large-scale networks.

In this case, geospatial methods can be used as an alternative approach. Zhu et al. (2015) developed and updated (Zhu et al., 2017) a liquefaction model based on geospatial characteristics, such as slope, elevation or distance to a water body. As the aim of this approach was the creation of a tool for rapid estimation of the extent of liquefaction in order to support rapid response and emergency planning, only variables which were easily accessible prior to any event were considered.

This paper focuses on the application of geospatial liquefaction susceptibility models for New Zealand to assess the exposure of national infrastructure networks. Here we focus on state highways, rail and the power transmission network. The paper also compares parts of the transportation and electricity transmission networks in New Zealand to evaluate contributing factors such as earthquake likelihood and infrastructure criticality.



Fig. 1 Liquefaction susceptibility map of New Zealand based on the geospatial model of Zhu et al. (2017)

2 GEOSPATIAL LIQUEFACTION MODEL

The Zhu et al. geospatial liquefaction model relies on a set of 18 variables which are related to factors most relevant to liquefaction: soil properties (relative density), water table depth (saturation), and ground shaking (load). To correlate these variables with liquefaction occurrence, case history data from 22 different earthquakes in the United States, Japan, New Zealand and Asia were obtained. Five events where liquefaction did not manifest within the same areas were also assessed to account for low intensity shaking events, in which liquefaction is unlikely to occur. The consideration of both scenarios maintained the data's completeness and increased the accuracy of the model. Since most liquefaction has manifested in coastal areas, the primary model was biased, making it less applicable to non-coastal regions. Therefore, a modified model with a different arrangement of variables was introduced for global implementation (Zhu et al., 2015; Zhu et al., 2017).

For soil properties and saturation, the bestperforming variables were *slope-derived* V_s30 (shearwave velocity over the first 30 m), *water table depth*, *distance to coast, distance to river, distance to closest water body*, and *precipitation. Peak ground velocity* (PGV) proved to be most suitable for characterizing ground shaking intensity. Interaction effects among variables, e.g. between *distance to coast* and *distance to rivers*, were also considered and improved the overall performance of the model. (Zhu et al., 2017)

Using logic regression, liquefaction probability was estimated and mapped for all events from the dataset. Comparing the predictions of both models with the actual observations showed several discrepancies, revealing the limitations of the approach. One reason for inaccurate results was the fact that site specific characteristics and other contributing factors (e.g. soil plasticity) were not included due to their restricted accessibility. Beyond that, the global model did not perform as well as the regional (coastal) model, indicating that variables related to soil saturation were the driving factor for liquefaction occurrence. Despite its limitations, the model of Zhu et al. (2017) provides useful results, especially considering the cost and time required to collate traditional in-situ methods across such a broad area (Maurer, 2017). It is therefore the best tool for assessment of liquefaction on a national scale and to estimate the potential liquefaction-induced damage to New Zealand infrastructure networks.

Based on the global model, a susceptibility map of New Zealand at a 100 m grid spacing was created (Fig. 1). Instead of the global Vs30 model, this approach made use of a recently developed New Zealand-specific V_s30 model (currently unpublished). Following the classification of Zhu et al. (2017), the susceptibility data can be interpreted by introducing the categories very low (white), low (green), moderate (yellow), high (orange), and very high (red). The map shows areas of high susceptibility in the centre of the North Island (Waikato, Bay of Plenty) and along the West coast of the South Island. These are areas with a lack of site specific investigation data, and also align with areas where the liquefaction susceptibility of deposits is the focus of current research (Tauranga City Council, 2016; Wahab & Clayton, 2017). As such, according to this geospatial model, the infrastructure in these districts may be exposed to liquefaction effects, and will be the focus of further analysis in this paper.

3 INFRASTRUCTURE NETWORKS

The functionality of national infrastructure networks is essential to provide services such as transportation and power transmission. Because of their geographic distribution, they are exposed to a range of natural hazards. Another important factor is the topography of New Zealand: The disruption in one location can often have widespread implications across the network. In the event of an earthquake, liquefaction-induced lateral spreading and ground deformation are the main causes of infrastructure damage. The impact varies between superficial changes, which do not interfere with the network's functionality, and a total failure of the system



Fig. 2 Infrastructure networks of New Zealand



Fig. 3 Liquefaction susceptibility of New Zealand infrastructure

(Mian et al., 2013; Ministry of Business, Innovation & Employment, 2017).

This paper analyses New Zealand state highways, rail network and the power transmission network (Fig. 2). State highways represent only 12% of the entire road system, but account for up to 50% of all motor vehicle travel distance. Facing a growing population, increasing freight transport and tourist travel needs, the state highways are a key network for New Zealand. Similar challenges apply to the rail network, which carries around 15% of national freight and is predicted to experience a 70% increase in freight movement during the next two decades (Ministry of Transport, 2011). According to the New Zealand Lifelines Council (2017), most utilities are highly dependent on electricity, underlining the importance of the power transmission network. Although backup generators are very common to secure constant power supply, a large-scale outage would result in subsequent outages for many lifeline services.

To incorporate infrastructure networks with liquefaction susceptibility, publically available data sets from the NZ Transport Agency (state highways), Land Information New Zealand (rail, bridges) and Transpower New Zealand Limited (power transmission) were used. In order to suit the data type of the susceptibility map, all infrastructure systems were modelled as point features. Linear networks were split into segments of 100 m, each represented by a centre point. In the assigning process, an infrastructure point simply adopted the value of the closest susceptibility point on the map.

Modelling the bridges of state highways and rail proved to be complex; Since the source data was in polyline format, three points were chosen to mark both ends (abutments) and the centre. The abutments are the most vulnerable part of the bridge; their susceptibility values determine the performance of the whole structure. The centre point, on the other hand, was chosen to illustrate the location more accurately on the map.

The power transmission network was characterised using the location of poles and pylons, as the functionality of the transmission lines are dependent on these structures. Locations of sites, representative of generation facilities and substations, were also assessed. A small overall length of subsurface cables are present in urban areas (e.g. Auckland), which are directly exposed to liquefaction (Transpower New Zealand Limited, 2018). For a detailed analysis at a local scale, which goes beyond the scope of this paper, buried transmission lines should be considered.

4 SUSCEPTIBILITY ANALYSIS

Using the liquefaction susceptibility map for each infrastructure network, this section provides a short analysis, comparing outputs and looking at two examples for further interpretation. An overview of the liquefaction susceptibility categories for all infrastructure types is shown in Fig. 3.

For state highways and rail, the results are very similar, which may be because rail follows the state highways at a number of locations (Fig. 2). The relatively high percentage of infrastructure sections with "moderate" to "very high" susceptibility (74.3% for state highways, 80.9% for rail) is because a large proportion of the networks are located close to the coast and across alluvial plain areas. For the assessment of liquefaction-induced damage, particular attention should be paid to areas where state highways and rail coexist, because it is very likely that both networks will be affected in the event of an earthquake.

Irrespective of the network, bridges lead to higher susceptibility results with 90% of state highway bridges and 90% of rail bridges being assigned a "moderate" to



Fig. 4 Liquefaction susceptibility of the BHL-WHN line (North) and the Inter-Island line (South). The map shows both transmission sites and structures, while the chart only represents structures.

"very high" category. Bridges often span rivers, where soil is alluvial and saturated, which is the primary indicator for liquefaction to occur (Youd, 1993). However, given the variability of soil deposit characteristics in these locations, further investigations are necessary to confirm these classifications.

Power transmission sites and structures show significantly lower susceptibilities. One reason for this is the concentration of transmission structures on mountainous terrain and/or away from the coast, which decreases the exposure to liquefaction compared to the transport network (but may increase the amplification of ground shaking or the exposure to other hazards, such as landslides).

Using susceptibility maps allows an overall comparison of infrastructure networks. Future research could focus on adding other networks (e.g. local roads or water pipes) and analysing correlations among all components. Besides the general assessment on a national level, local hot spots could also be of interest.

4.1 Earthquake likelihood

High susceptibility does not necessarily result in high risk. Areas which are classified as very susceptible, but not prone to strong ground shaking, may be less relevant than areas of low susceptibility with a high exposure to earthquakes (Glassey & Heron, 2012). Zhu et al. (2017) assumed that a PGV of at least 3 cm/s is required to initiate the liquefaction process. To illustrate the importance of earthquake likelihood, two transmission lines will be discussed in detail (Fig. 4): (1) the BHL-WHN line between Brownhill (Auckland) and Whakamaru North (Waikato), one of the major high voltage alternating current lines in New Zealand, providing power to Waikato, Auckland and Northland; (2) the Inter-Island line, which starts in Haywards (Wellington) and crosses most parts of the South Island down to Benmore (Canterbury). The Inter-Island connects the power network of both islands and secures a balanced availability and demand ratio. It highly depends on the substation in Haywards, the main power supplier of Wellington (New Zealand Lifelines Council, 2017). As illustrated in charts of Fig. 4, the structures of line have BHL-WHN similar liquefaction the susceptibilities as the average facilities in Fig. 3. In contrast, the structures of the Inter-Island show a decreased range of "high" (-11.1%) and "very high" (-5.5%) values, indicating they are less susceptible to liquefaction. This also applies to the transmission sites: While the substation in Whakamaru (BHL-WHN line) is very susceptible ("high"). Inter-Island sites result in mostly "very low" susceptibilities (except for the power cable terminal in Oteranga Bay, Wellington).

Based on the susceptibility results alone, the BHL-WHN line appears to carry a greater risk in terms of liquefaction exposure. However, it is located in an area where strong earthquakes are unlikely. For the Inter-Island, on the other hand, the likelihood of ground shaking is considered high due to its proximity to a number of active fault sources (Stirling et al., 2012). Therefore, by taking both these factors into account, the risk of liquefaction-induced damages is expected to be lower for the Inter-Island line.

The example illustrates that the assessment of the susceptibility map alone will lead to incorrect outcomes. The inclusion of ground motion data for different earthquake scenarios and seismic hazard estimates is indispensable for a proper analysis of the liquefaction hazard.

4.2 Infrastructure criticality

Partially or fully damaged infrastructure can cause a diversity of consequences on the economy and society. Some networks are more relevant than others, making infrastructure significance or criticality an important factor for the evaluation of the potential impact of liquefaction induced damage. This will be demonstrated by comparing two state highways in the South Island, which are both exposed to the effects of an Alpine Fault earthquake: (1) SH1, which starts in Picton and runs down the East coast to Bluff while passing several sea ports and populated towns and cities, such as Christchurch and Dunedin; (2) SH6, which starts in



Fig. 5 Liquefaction susceptibility of state highway SH1 (East) and SH6 (West)

Blenheim crossing over to Westport and running south along the West Coast. After Haast, the SH6 veers inland to pass Queenstown, ending in Invercargill. Fig. 5 presents the liquefaction susceptibility of both state highways incl. the locations of sea ports on the South Island. While SH1 appears to have a nearly homogenous distribution, SH6 shows a cluster of "very high" susceptibilities within the West Coast area. The differences are also illustrated in the charts: Compared the results in Fig. 3, the range of "high" to susceptibilities increased for SH1 (+7.2%), while the number of "very high" susceptibilities dropped considerably (-6.9%). SH6 clearly stands out in the category "very high": Around 20% of the highway is very susceptible to liquefaction.

The comparison of both state highways indicates that attention should be paid to the critical section of SH6 along the West Coast. However, in terms of infrastructure criticality, it becomes clear that SH1 has a strikingly higher traffic volume (in parts more than 10000 vehicles per day) and links the majority of sea ports to the national transport system (Ministry of Transport, 2011). Therefore, although the liquefaction may be lower along SH1, the impact of failure on national transportation and economy would likely be a lot more significant. The example emphasizes the importance of infrastructure significance and criticality during hazard and risk assessments. This requires a proper understanding of the diverse and complex factors contributing to a network's economic and social value.

5 CONCLUSION

The geospatial model of Zhu et al. (2017) provides a useful tool to develop a national-scale liquefaction susceptibility map of New Zealand. Infrastructure for transportation and power was integrated to the map, showing that (1) state highways and rail have similar susceptibility results due to their common location, (2) bridges are more susceptible than other structures, because they are often located adjacent to rivers on alluvial deposits, and (3) transmission sites and structures are less susceptible to liquefaction than transportation networks as they are often situated across hills and away from alluvial deposits or coasts.

The comparison of different networks, discussed in 4.1 and 4.2, underlines the fact that creating a nationalscale susceptibility map is only the first step to an adequate liquefaction risk assessment. Comprehensive data on ground shaking, studies of infrastructure vulnerability, and methods to measure infrastructure criticality are required to fully understand the potential impacts of infrastructure networks that are exposed to liquefaction.

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REFERENCES

- Boulanger, R. W.; & Idriss, I. M. (2014). CPT and SPT based liquefaction triggering procedures. Report No. UCD/CGM.-14/01, Center for Geotech. Modelling, Civil & Environmental Eng., UC Davis, CA.
- Cubrinovski, M. (2013). Liquefaction-induced damage in the 2010-2011 Christchurch (New Zealand) earthquakes. International Conference on Case Histories in Geotechnical Engineering (Apr 29th – May 4th).
- Glassey, P. J.; & Heron, D. W. (2012). Amplified ground shaking and liquefaction susceptibility, Invercargill City. GNS Science Consultancy Report 2012/2014.
- Maurer, B. W. (2017). Field-testing liquefaction models based on geospatial vs. geotechnical data. *Proceedings of the 6th International Young Geotechnical Engineers' Conference* (*iYGEC6*).
- 5) Mian, J. F.; Kontoe, S.; & Free, M. (2013). Assessing and managing the risk of earthquake-induced liquefaction to civil infrastructure. *Handbook of Seismic Risk Analysis and Management of Civil Infrastructure Systems*, pp. 113-138, Woodhead Publishing. DOI: https://doi.org/10.1533/9780857098986.1.113

- Ministry of Business, Innovation & Employment (2017). Planning and engineering guidance for potentially liquefaction-prone land.
- 7) Ministry of Transport (2011). Connecting New Zealand A summary of government's policy direction for transport.
- New Zealand Lifelines Council (2017). New Zealand lifelines infrastructure vulnerability assessment: Stage 1. URL: <u>https://www.civildefence.govt.nz/assets/Uploads/lifelines/National-Vulnerability-Assessment-Stage-1-September-2017.pdf</u> (accessed 08.08.2018)
- Stirling, M. W.; McVerry, G. H.; Gerstenberger, M. C.; Litchfield, N. J.; Van Dissen, R. J.; Berryman, K. R.; Barnes, P.; Wallace, L. M.; Villamor, P.; Langridge, R. M.; Lamarche, G.; Nodder, S.; Reyners, M. E.; Bradley, B.; Rhoades, D. A.; Smith, W. D.; Nicol, A.; Pettinga, J.; Clark, K. J.; & Jacobs, K. (2012). National seismic hazard model for New Zealand: 2010 update. *Bulletin of the Seismological Society of America*, Vol. 102, No. 4, pp. 1514-1542. DOI: http://doi.org/10.1785/0120110170
- Tauranga City Council (2016). Liquefaction assessment of the Wairakei/Te Tumu area. Prepared by Tonkin&Taylor. Job number 851988.v0. May 2016.
- 11) Transpower New Zealand Limited (2018). Transpower transmission network: North Island. January 2018. URL: <u>https://www.transpower.co.nz/sites/default/files/plainpage/attachments/Transmission-map-north-island18.pdf</u> (accessed 12.08.2018)
- 12) Wahab, H., & Clayton, P. J. (2017). Liquefaction assessment for an urban roading project in the Bay of Plenty. 20th NZGS Geotechnical Symposium.
- 13) Youd, T. L. (1993). Liquefaction-induced damages to bridges. *Transportation Research Record*, No. 1411, pp. 35-41.
- 14) Zhu, J.; Daley, D.; Baise, L. G.; Thompson, E. M.; Wald, D. J.; & Knudsen, K. L. (2015). A geospatial liquefaction model for rapid response and loss estimation. *Earthquake Spectra*, Vol. 31, No. 3, pp. 1813-1837. DOI: <u>https://doi.org/10.1193/121912EQS353M</u>
- 15) Zhu, J.; Baise, L.; & Thompson, E. (2017). An updated geospatial liquefaction model for global application. *Bulletin* of the Seismological Society of America, Vol. 107, No. 3, pp. 1365-1385. DOI: <u>https://doi.org/10.1785/0120160198</u>